

South Cell at Woy Woy Waste Management Facility

Technical Report 2 – Leachate Infiltration Modelling and Water Balance

Central Coast Council 06 December 2023



| Project name Document title Project number | | Detailed Design and Documentation for South Landfill Cell at Woy Woy | | | | | | |
|--|---|---|----------------------------------|-----------|--------------------|--------------|---------|-----------|
| | | South Cell at Woy Woy Waste Management Facility Technical Report 2 – Leachate Infiltration Modelling and Water Balance 12595244 | | | | | | |
| | | | | | | | | File name |
| Status Revision | | Author | Reviewer | | Approved for issue | | | |
| Code | | | Name | Signature | Name | Signature | Date | |
| S4 | 0 | S. Kentwell | C. Nivison- Smith A. Dixon | April | D. Gamble | David land C | 6/12/23 | |
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1. Introduction

1.1 Overview

Central Coast Council (Council) owns and operates the existing Woy Woy Waste Management Facility (WMF) located on Nagari Road, Woy Woy. The WMF is the primary waste disposal facility for the southern Central Coast community and has operated since 1974. The WMF operates in accordance with Environment Protection Licence (EPL) No. 6053. The EPL permits resource recovery, waste disposal (application to land) and waste storage and authorises landfilling of up to 100,000 tonnes per year of putrescible and non-putrescible general solid waste, tyres and asbestos.

Key components of the existing WMF include:

- Weighbridge and office/education centre
- Current active landfill cell and tipping area
- Transfer station
- Garden organics (GO) facility
- Excavation and stockpiling area
- Stormwater and leachate management infrastructure

In 2020 Council commissioned the 'Woy Woy Waste Management Facility – Development Strategy' (SMEC, 2020) (the 'Development Strategy') to guide the future use and development of the facility. The Development Strategy identified the existing excavation and stockpile area at the southern end of the WMF as the location for the next waste cell (known as the new 'South Cell').

Council is now proposing to develop the new South Cell to optimise the remaining landfill air space at the WMF and ensure that the WMF remains open for as long as possible to accept putrescible waste from the Local Government Area (LGA).

The construction of the proposed new South Cell is required to be completed and able to receive waste when the current tipping area reaches capacity in mid to late 2024. Construction would commence following receipt of planning approval and be completed in two stages. Each stage is expected to take four to six months.

The project is deemed regionally significant development (RSD) and is subject to approval by the Hunter and Central Coast Regional Planning Panel under the *NSW Environmental Planning and Assessment Act* 1979 (EP&A Act).

This report has been prepared by GHD Pty Ltd (GHD) as part of the environmental impact statement (EIS) for the project. The EIS has been prepared to support the application for approval of the project and address the environmental assessment requirements of the Secretary of the NSW Department of Planning and Environment (the SEARs) dated 24 August 2023.

1.2 The project

1.2.1 Location

The project would be located within the existing Woy Woy WMF. The WMF is about 10 kilometres south of Gosford across Brisbane Water, within the Central Coast LGA (refer Figure 1.1).

The WMF site consists of:

- Lot 110 DP 755251
- Lot 1 DP 126813
- Lot 1 DP 654885

The South Cell (the project site) is about five hectares in area and located on the southern portion of the WMF. It comprises part of Lot 110 DP 755251.

1.2.2 Key features

Key features of the project include:

- Cell construction including excavation and earthworks to form the base of the cell and lining installation
- Development of associated access, stormwater, and leachate management infrastructure
- Continuation of current landfilling operations in the new cell location
- Capping, closure, and rehabilitation

The project is expected to provide up to approximately an additional 920,000 cubic metres of airspace or 7.7 years of filling capacity (based on current filling rates). It is also expected to generate additional cell construction and cover materials for the ongoing landfilling operations.

No change is proposed to the existing approved annual disposal capacity or waste types as per EPL 6053.

The other existing operations (weighbridge and office/education centre, transfer station, GO facility etc) at the WMF would continue to be operated in conjunction with the project.

Further information on the project is provided in the EIS.

The project site layout is shown in Error! Reference source not found.

1.2.3 Construction overview

Construction of the project would be subject to the methods proposed by the construction contractor, but is expected to involve the following:

- Site establishment: establishment of site environmental controls including sediment and erosion controls
- Earthworks: excavation and grading along the base of the landfill cell in accordance with the requirements of the *Environmental Guidelines: Solid waste landfills* (NSW EPA, 2016)
- Lining and gravel placement: installation of basal, batter and sidewall liners systems
- Development of ancillary infrastructure including access roads, leachate, gas and water management infrastructure

Construction is expected to take about three months to complete.

The construction activities would be carried out during the following hours, consistent with the recommended standard hours of the *Interim Construction Noise Guideline* (NSW DECC, 2009):

- 7 am to 6 pm Monday to Friday
- 8 am to 1 pm Saturdays
- No work on Sundays or Public Holidays

The construction workforce is expected to range between five and ten workers per day.

Further information on the construction of the project is provided in the EIS.

1.3 Secretary's Environmental Assessment Requirements

The specific SEARs addressed in this report are summarised in Table 1.1.

Table 1.1 SEARs relevant to this assessment

| Requirement | Where addressed in this report | |
|--|--------------------------------|--|
| Details of proposed leachate and gas management and monitoring | Section 7 | |

1.4 Purpose of this report

This purpose of this report is to outline the methodology, assumptions and results of the infiltration modelling and a leachate water balance for existing and future stages of the WMF landfill operations, including the South Cell.

1.5 Scope of this report

Specifically, this report includes:

- Review of existing leachate management system.
- Description of infiltration modelling, including methodology and results.
- Description of leachate water balance modelling, including methodology and results.
- Overview of proposed leachate management measures for the South Cell.

The infiltration modelling and leachate water balance modelling described in this report were completed in accordance with NSW EPA's *Environmental Guidelines: Solid Waste Landfills* (2016).

1.6 Limitations

This report: has been prepared by GHD for Central Coast Council and may only be used and relied on by Central Coast Council for the purpose agreed between GHD and Central Coast Council as set out in Section 1.3 of this report.

GHD otherwise disclaims responsibility to any person other than Central Coast Council arising in connection with this report. GHD also excludes implied warranties and conditions, to the extent legally permissible.

The services undertaken by GHD in connection with preparing this report were limited to those specifically detailed in the report and are subject to the scope limitations set out in the report.

The opinions, conclusions and any recommendations in this report are based on conditions encountered and information reviewed at the date of preparation of the report. GHD has no responsibility or obligation to update this report to account for events or changes occurring subsequent to the date that the report was prepared.

The opinions, conclusions and any recommendations in this report are based on assumptions made by GHD described in this report. GHD disclaims liability arising from any of the assumptions being incorrect.

The opinions, conclusions and any recommendations in this report are based on information obtained from, and testing undertaken at or in connection with, specific sample points. WMF conditions at other parts of the WMF may be different from the WMF conditions found at the specific sample points.

Investigations undertaken in respect of this report are constrained by the particular site conditions, such as the location of buildings, services and vegetation. As a result, not all relevant site features and conditions may have been identified in this report.

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Accessibility of documents

If this report is required to be accessible in any other format, this can be provided by GHD upon request and at an additional cost if necessary.



0 140 280 420 560 Metres Map Projection: Transverse Mercator Horizontal Datum: GDA 1994 Grid: GDA 1994 MGA Zone 56



Central Coast Council South Cell at Woy Woy WMF Leachate Infiltration Modelling and Water Balance

Site location

Revision No. 0 Date 10/10/2023

FIGURE 1.1

\lghdnet\ghd\AU\Newcastle\Projects\22\12595244\GIS\Maps\Deliverables\12595244_EIS.aprx Print date: 10 Oct 2023 - 19:19 Data source: GHD: Site Boundary (2023), Survey Data (2023). World Topographic Map: Esri, HERE, Garmin, Foursquare, METINASA, USGS World Hillshade: Esri, Geoscience Australia, NASA, NGA, USGS Nearmap WMS Server: . Created by: dbbanatin

2. What is leachate?

Leachate is liquid/water which has been in contact with the landfilled waste at the WMF, resulting in "leaching" of substances from the waste into this water. Due to its composition, leachate must be managed in a specific way, from collection to eventual disposal.

Leachate is managed separate to other surface water flows at a landfill, including:

- Clean water diverted around any waste and/or disturbed areas.
- Sediment laden water that has been entrained only by sediment from disturbed areas (and no other contaminants).

For this delineation, where virgin excavated natural material (VENM) is used as daily, intermediate and final cover, any water runoff can be managed as one of the surface water flows above and does not need to be managed as leachate (unless leachate were to enter it via seepages from a batter or similar).

In addition, the area located on the platform of the WMF is used for the temporary storage of garden organics (GO), referred to as the GO facility. While there is no composting or processing undertaken here, Condition O7.1 of the EPL 6053 identifies this area as the 'organics processing area' and references its design plans titled 'Central Coast Council Woy Woy WMF – Organics Processing Area – Revision A – Drawing Numbers 22-20113-C001 to C004, Drawing 22-20113-C011 to C018, Drawing 22-20113-C021 and 22-20113-C080'. It is noted that Council intends to remove this clause from their EPL.

This area, along with the transfer station, currently discharges to the sediment-laden management system where it is collected for re-use or treated/discharged accordingly. As a result of the low residence time of materials and the absence of higher risk materials and processes (e.g., food waste or composting), runoff from this area may be characterised as stormwater and could potentially continue to be discharged to the stormwater system. Monitoring and testing is currently being undertaken by Council to confirm this outcome.

A Trigger Action Response Plan (TARP) has been developed and is included in the Soil and Water Impact Assessment (separate to this report) with appropriate actions based on results of future water quality monitoring. In extreme circumstances, this TARP may require diversion of the runoff from the GO facility and transfer station to the leachate management system. Specific to this leachate water balance, potential diversion of these flows to the leachate management system has been considered in terms of estimated leachate quantities, to confirm the system is adequate for this scenario.

3. Regulatory guidance

3.1 NSW Landfill Guidelines

The NSW EPA's *Environmental Guidelines: Solid Waste Landfills* (2016) – henceforth referred to as the NSW Landfill Guidelines – provide guidance for the environmental management of landfills in NSW by specifying a series of 'Minimum Standards'. They involve design and construction techniques, effective site operations, monitoring and reporting protocols, and post-closure management. These guidelines have been considered with reference to the leachate water balance assessment and development of leachate management measures for the South Cell.

3.2 Development consent

In 1994 a legal review of the development consent for the Woy Woy WMF (Dawson, 1994) found that a consent was obtained of the then Health Commission to use the WMF as a solid waste disposal depot.

A new development consent would be sought for the project. The project is deemed to be regionally significant development (RSD) in accordance with Clause 7(1)(c) and Clause 3 in Schedule 6 of *State Environmental Planning Policy (Planning Systems) 2021* (Planning Systems SEPP) and it is a development for the purposes of a waste management facility or works that meets the requirements for designated development under the Environmental Planning and Assessment Regulation 2021, Schedule 3, section 45 as well as being Council related development with a capital investment value over \$5 million. The project therefore requires assessment and approval in accordance with Part 4, Division 4.3 of *the Environmental Planning and Assessment Act 1979* (NSW) (EP&A Act) for determination by the Hunter and Central Coast Regional Planning Panel. An environmental impact statement (EIS) is required to be submitted as part of the application for development consent.

3.3 Environment protection licence

Table 3.1 lists the relevant conditions of EPL 6053 that were considered as part of the concept design. As the project is outside the approved landfill footprint, it is expected that the design would need to comply with the NSW Landfill Guidelines which would supersede certain conditions below, such as lining and capping requirements.

| Conditio | on Requirements |
|----------|--|
| O5 | Processes and Management |
| O5.1 | The sedimentation and leachate dams must be maintained to ensure that their design capacity is available for the storage of stormwater/leachate. |
| O5.4 | A leachate barrier system must be installed on each surface within the premises to be used for the storage of leachate. |
| O6 | Waste Management |
| O6.1 | The sedimentation and leachate dams must be maintained to ensure that their design capacity is available for the storage of stormwater/leachate. |
| O6.2 | A leachate barrier system and leachate collection system as detailed in Section 7.2 of the LEMP must be installed on each surface within the premises to be used for the disposal of waste. This condition does not apply to any surface used for the emplacement of waste before 1 July 1998 as described by Section 7.2 of the LEMP. |
| O6.3 | The liner and sub-grade must be installed above the groundwater table. |
| O6.4 | A leachate barrier system must be installed on each surface within the premises to be used for the storage of leachate. |
| O6.8 | The licensee must manage the disposal of waste at the premises in accordance with the progressive filling plan Section 6.3 of the LEMP. |

Table 3.1 Relevant EPL conditions

| Conditio | n Requirements | |
|----------|---|--|
| O6.9 | The licensee must ensure that the landfill cells are capped progressively and specifically at times when the level of waste reaches final heights as detailed in Section 10 of the LEMP. | |
| O6.10 | Final capping at the premises must comprise of two layers in the order of installation - a sealing layer and a revegetation layer. Final capping must be in accordance with the capping profile and the five year capping survey prepared by Chase, Burke and Harvey Surveying (June 2013). | |
| O6.11 | The cap must comprise a firm stable smooth foundation layer overlaid by a clay sealing layer which has a permeability of no more than 10 ⁻⁸ metres per second, and a minimum thickness of 900mm overlaid by a topsoil revegetation layer with a minimum thickness of 150mm. | |
| O6.13 | Cover material must be: | |
| | (a) Daily Cover | |
| | Cover material must be applied to a minimum depth of 15 centimetres over all exposed landfilled waste prior to ceasing operations at the end of each day and must be either | |
| | (i) virgin excavated natural material; or | |
| | (ii) an approved synthetic cover. | |
| | (b) Intermediate Cover | |
| | Cover material must be virgin excavated natural material and must be to a depth of 30 centimetres over surfaces of the landfilled waste at the premises which are to be exposed for more than 90 days | |
| | (c) Cover material Stockpile | |
| | At least two weeks of cover material must be available at the premises under all weather conditions. The material may be won on site, or alternatively a cover stockpile must be maintained adjacent to the tip face. | |

3.4 Landfill management plan

The WMF operates in accordance with a Landfill Management Plan (LMP) prepared by URS (2012). As described above, a number of the EPL conditions reference the LMP. This includes the current approved final landform, as shown in Figure 3.1.



Figure 3.1 Filling plan from LEMP (URS, 2012)

4. Existing leachate management system

4.1 Minimisation

Daily and intermediate cover material is used to limit infiltration of rainfall into the landfilled waste, as per Condition O13.1 of the WMF's EPL. Excavated material from the South Cell is currently being used as a cover material source.

Council has indicated that final capping has been installed across finished portions of the existing landfill, in line with the requirements of conditions O6.9, O6.10 and O6.11.

4.2 Containment

URS (2012) outlines that historical cells A1 to A5 are unlined and do not have a leachate barrier system. However, they are constructed within medium to high strength sandstone within a network of perimeter clay bunds and internal clay cell walls (SMEC, 2020).

Based on URS (2012), Cells 1 and 2 were constructed with a clay and geosynthetic clay liner (GCL), comprising:

- Cell base liner (top to bottom):
 - 600 mm thick clay protection layer
 - GCL sealing layer
 - 100 mm thick clay subgrade improvement layer
- Cell batter liner
 - 900 mm thick clay sealing layer

The Western Cell was constructed with a clay and GCL (top to bottom), comprising:

- 300 mm thick soil protection layer
- GCL sealing layer
- 300 mm thick clay subgrade improvement layer



Figure 4.1 Existing cell locations (URS, 2012)

4.3 Collection and transfer

As documented in SMEC (2020), a leachate collection system has been constructed within the historical landfill cells, located on the down slope side of the landfilled areas along the extremities of the WMF. The leachate collected in the south and northwest is directed to sumps where it is pumped to the leachate dam in the north of the WMF, shown in Figure 4.2.

Leachate collected in Cells 1 and 2 drains to the leachate dam via gravity. The cells are graded at a minimum of 1(V):80(H) on the cell base, and 1(V):20(H) along the main leachate drainage lines to the leachate dam. Cells 1 and 2 are lower than the historical cells, allowing leachate to be collected by the new leachate collection systems.

Leachate collected in the newer Western Cell also gravity drains to the leachate dam in the north. The leachate collection system for the Western Cell comprises a herringbone structure of slotted pipes within the fill area at a spacing of 20 m. The collection pipes feed to a solid leachate drainage pipe, running directly to the leachate dam.



Figure 4.2 WMF layout development plan (SMEC, 2020)

4.4 Storage and disposal

The leachate dam was constructed in February 1999 and is lined with HDPE, with an approximate capacity of 1,000 kL. Stored leachate is discharged from the dam directly to the Woy Woy Sewerage Treatment Plant (STP) located to the north of the WMF when the leachate in the dam reaches a specified level. A recent survey of the leachate pond is provided in Figure 4.3 below (designated 'L1', noting 'N1' is a sediment pond). Alongside the South Cell development, Council is upgrading the sewer disposal pipework from the dam to the Woy Woy STP.

It is understood that there are no current restrictions on the leachate volumes or quality accepted by the treatment plant (SMEC, 2020). No other leachate disposal mechanisms exist at the WMF other than evaporation from the leachate dam and discharge to sewer.

Further to the above, it is understood that Council has historically utilised the sewer disposal for sediment laden water disposal during significant wet weather events. However, Council is seeking to move away from this practice as part of the development of the South Cell.



Figure 4.3 Leachate pond survey (Barry Hunt Associates, 2020)

4.5 Monitoring

Relevant to leachate management, condition M2 of the WMF's EPL requires quarterly and annual monitoring of:

- Five groundwater monitoring bores.
- The leachate storage pond.

Further information has been sought from Council to estimate groundwater levels at the WMF and potential interaction with historical unlined cells, to be considered in future updates to this report.

Based on Council feedback, the existing leachate flow meters onsite do not operate correctly, as such no leachate volumetric data is available at the time of this report. Council is seeking to install a leachate flow meter on a secondary line and pump to support this assessment. Where possible, the data from this flow meter would be considered as part of this leachate water balance and its calibration in future updates to this report. Further information is also being sought on the leachate volumes being received and recorded at the treatment plant, to be considered in future updates to this report.

5. Infiltration modelling

5.1 Methodology

The United States Environmental Protection Agency's Hydrologic Evaluation of Landfill Performance (HELP) model was used to provide a comparative evaluation of infiltration through the various cover and cap profiles across the WMF for all stages of development proposed. The model considers rainfall, evapotranspiration and stormwater run-off. The use of this software is endorsed as a suitable method within the NSW Landfill Guidelines.

The data was analysed for the 50% Average Exceedance Probability (AEP) rainfall (median) year (2008 – 1190.5 mm) and 10% AEP rainfall (wet) year $(1952 - 1701.4 \text{ mm})^1$ to estimate annual leachate generation rates.

5.2 Input data

5.2.1 General

Two key inputs were required for the infiltration modelling:

- 1. Climate data (specifically rainfall, temperature and evaporation data)
- 2. Cover and capping profiles (including material type and depth)

5.2.2 Climate data

The model requires a comprehensive set of daily climate data to represent the WMF. Rainfall, evaporation and temperature data was obtained from SILO, hosted by The Science Delivery Division of the Queensland Department of Science, Information Technology, Innovation and the Arts (DSITIA). SILO is a database of Australian climate data from 1889 to the present which provides daily meteorological datasets for a range of climate variables, constructed from observational data obtained from the Bureau of Meteorology (BOM) and other suppliers (e.g., private landholders, natural resource management groups, commercial organisations and Government agencies).

Patched point data uses real historical data, where available, and patches missing or suspect data with interpolated daily observations data. SILO data was extracted on 7 February 2023 from the data drill point of coordinates (-33.50, 151.30). The identified period (1923-2022) was selected as it provides a representation of 100 years of storm events so that a wide range of potential rainfall events can be considered to select the applied rainfall events..

Data from the Mangrove Mountain Automated Weather Station (AWS) Bureau of Meteorology (BOM) weather station (No. 061375) located approximately 10 km northwest of the WMF was used for relative humidity and windspeed. The years of data for the relevant climatic parameters used are contained in Table 5.1.

| Parameter | Data source | Years |
|-------------------|-----------------------|--------------|
| Rainfall | SILO data drill point | 1923 to 2022 |
| Evaporation | SILO data drill point | 1923 to 2022 |
| Solar radiation | SILO data drill point | 1923 to 2022 |
| Temperature | SILO data drill point | 1923 to 2022 |
| Relative humidity | Mangrove Mountain AWS | 1944 to 2010 |
| Wind speed | Mangrove Mountain AWS | 1944 to 2010 |

| Table 5.1 | HELP modelling climatic parameters and years of data used |
|-----------|---|
| 10010 0.1 | The interest of a land the second s |

¹ Based on the 10% AEP rainfall using SILO grid point data for years between 1923 to 2022

5.3 Cover and capping profiles

5.3.1 General

Table 5.2 below identifies the modelling parameters associated with each of the cover and capping profiles proposed for the project. Unless otherwise specified, the standard HELP values for porosity, field capacity, wilting point and hydraulic conductivity have been utilised for the selected material types.

The slope grades and lengths have been extracted from a recent survey of the existing areas (December 2022, as supplied by Council) and the concept design for the project, which is being completed in parallel to this study. These would be updated progressively based on the ongoing design updates completed by GHD as part of the overall project to align with the final design documentation. Where relevant, the cover and capping profiles were split up into platform and batter areas to model these differing surfaces.

5.3.2 Cover profiles

Cover profiles are based on the requirements of the WMF's EPL, which align with the recommendations of the NSW Landfill Guidelines (hence is applicable to current operations and future operations in the project). A silty clay was modelled which is a similar material type to what has historically been utilised at the WMF (including crushed sandstone from WMF borrow pits).

5.3.3 Capping profiles

The WMF's EPL outlines a capping profile of clay (900 mm thick) overlain by topsoil (150 mm thick), as specified in capping profile and the five-year capping survey prepared by Chase, Burke and Harvey Surveying (June 2013). This has been included as Option 1 and is applicable to existing landfilled areas within the EPL footprint. Council feedback suggests this option was used across all capped areas in the existing WMF.

However, as the South Cell is a new development area and would be subject to a new consent, it is expected that the EPA would require capping to be line with the current version of NSW Landfill Guidelines. Hence a second option has been modelled in line with these guidelines and the concept design for the South Cell:

- Option 1: Final cap in accordance with the Capping Profile and the Five Year Capping Survey prepared by Chase, Burke and Harvey Surveying (2013), as per the WMF's EPL. Given the limited thickness of the revegetation layer for this option, calibration activities in future updates to this report would consider a higher permeability range for the clay material as part of a sensitivity analysis.
- Option 2: Final cap in accordance with the current NSW Landfill Guidelines, with GCL instead of clay as per the South Cell concept design.

In addition to the above, another profile was modelled specific to the GO facility given its alternative hardstand profile as identified by Council, which was akin to the Option 1 capping with hardstand materials overtopping instead of revegetation material.

The transfer station area was covered separate from the HELP modelling, as described in Section 6.4.

Table 5.2 Cover and capping arrangements

| Cover | Assumptions | Profile (top to bottom) |
|--|--|--|
| Daily cover | 0% runoff allowance No vegetation 0.1 m evaporative zone depth Slope grade 5% Slope length 50 m | 0.15 m thick daily cover – Silty clay (HELP soil profile #14) Underlying waste material |
| Intermediate cover – platform (unvegetated) | 50% runoff allowance No vegetation 0.2 m evaporative zone depth Slope grade 5% Slope length 225 m | 0.3 m thick intermediate cover – Silty clay (HELP soil profile #14) Underlying waste material |
| Intermediate cover – batter (unvegetated) | 50% runoff allowance No vegetation 0.2 m evaporative zone depth Slope grade 15% Slope length 90 m | |
| Intermediate cover – batter (vegetated) | 50% runoff allowance Poor stand of grass 0.2 m evaporative zone depth Slope grade 15% Slope length 90 m | |
| Final Cap Option 1 – platform | 75% runoff allowance Poor stand of grass 0.15 m evaporative zone depth Slope grade 5% Slope length 225 m | 0.15 m thick topsoil layer – Loam (HELP soil profile #8) 0.9 m thick sealing layer – Compacted clay (HELP soil profile #16, hydraulic conductivity K ≤ 10⁻⁸ m/s) 0.3 m thick intermediate cover – Silty clay |
| Final Cap Option 1 – batter | 90% runoff allowance Poor stand of grass 0.15 m evaporative zone depth Slope grade 15% Slope length 90 m | (HELP soil profile #14) – Underlying waste material |
| Final Cap Option 2 – platform | 75% runoff allowance Fair stand of grass 0.3 m evaporative zone depth Slope grade 5% Slope length 225 m | 0.2 m thick topsoil layer – Loam (HELP soil profile #8) 0.8 m thick subsoil layer – Sandy loam (HELP soil profile #10) LLDPE geomembrane (HELP profile #36) Geosynthetic clay liner (HELP soil profile |
| Final Cap Option 2 - batter | 90% runoff allowance Fair stand of grass 0.3 m evaporative zone depth Slope grade 15% Slope length 90 m | Geosynthetic clay liner (HELP soil profile #17) 0.3 m thick intermediate cover – Silty clay (HELP soil profile #14) Underlying waste material |
| Central area – GO facility | 75% runoff allowance No vegetation 0.15 m evaporative zone depth Slope grade 1% Slope length 80 m | 0.3 m thick hardstand cover – Sandstone (HELP soil profile #10) 0.9 m thick sealing layer – Compacted clay (HELP soil profile #16, hydraulic conductivity K ≤ 10⁻⁸ m/s) Underlying waste material |

5.4 Results

The results of the HELP modelling are contained in Appendix A and as a summary, as a percentage of rainfall infiltrating through the cover/capping profile, is included in Table 5.3.

The results for the daily and interim cover profiles are within expected levels, and result in higher infiltration compared to the capping profiles. The existing capping profile in the WMF's EPL produces significantly more infiltration compared to the proposed final capping for the project. This is expected given the proposed final capping utilises a composite geosynthetic material profile that includes materials with significantly improved sealing capabilities compared to the clay material currently being used.

| Cover / capping scenario | Rainfall scenario | Percentage infiltration (%) |
|-------------------------------------|------------------------------|-----------------------------|
| Daily cover | 50% AEP (2008) – median year | 65% |
| | 10% AEP (1952) – wet year | 77% |
| Interim cover (platform) | 50% AEP (2008) – median year | 27% |
| | 10% AEP (1952) – wet year | 37% |
| Interim cover (batter, unvegetated) | 50% AEP (2008) – median year | 27% |
| | 10% AEP (1952) – wet year | 37% |
| Interim cover (batter, vegetated) | 50% AEP (2008) – median year | 28% |
| | 10% AEP (1952) – wet year | 36% |
| Final capping – Option 1 (platform) | 50% AEP (2008) – median year | 12% |
| | 10% AEP (1952) – wet year | 9% |
| Final capping – Option 1 (batter) | 50% AEP (2008) – median year | 12% |
| | 10% AEP (1952) – wet year | 9% |
| Final capping – Option 2 (platform) | 50% AEP (2008) – median year | <1% |
| | 10% AEP (1952) – wet year | <1% |
| Final capping – Option 2 (batter) | 50% AEP (2008) – median year | <1% |
| | 10% AEP (1952) – wet year | <1% |
| Central area – GO facility | 50% AEP (2008) – median year | 3% |
| | 10% AEP (1952) – wet year | 2% |

Table 5.3 HELP model results (percentage infiltration)

6. Leachate water balance

6.1 General

Leachate water balance modelling was undertaken utilising the results of the infiltration modelling presented in Section 5 and the assumptions described below. The water balance was used to estimate leachate generation across the existing and future stages of the WMF (including the South Cell) and inform the proposed leachate management measures for the South Cell. It does not consider leachate volumes should it be mounded in the landfill. This is addressed separately is section 7.7 for consideration if needed when later calibrating the water balance.

6.2 Surface water run-on and run-off

Cut off drains are located on the east and west ridges, to convey external catchment flows and discharge to a tributary of Woy Woy Creek in the northwest of the WMF.

Sediment laden flows from operational areas are directed to the sediment ponds at the northern and southern ends of the WMF, where it is reused for WMF operations or disposed of via evaporation. In heavy rainfall events, surface water in the northern pond discharges to a creek located to the west of the WMF and surface water in the southern ponds discharge towards Patonga Creek.

A number of additional improvements are being proposed as part of *Technical Report 1 - Soil and Water Impact Assessment*, being completed alongside the leachate water balance and concept design of the South Cell. Based on the above these proposed improvements, it is assumed that no additional leachate is generated via run-off or run-on of surface water flows.

In line with Section 4.4, it is assumed that the sewer disposal is not utilised for other disposal measures such as for sediment laden water.

6.3 Groundwater inflow

Insufficient information is available on the base levels of the historical landfill cells to determine if groundwater inflow is likely and needs to be incorporated in the leachate water balance. As such, this has been excluded from the volumetric estimates, however the potential impacts are discussed as part of the results section below.

The South Cell is proposed to be located above the groundwater table (discussed further in *Technical Report 1 - Soil and Water Impact Assessment*) and include a groundwater drainage system, hence no groundwater inflow into this cell has been considered in the leachate water balance.

6.4 Unlined areas

As there are unlined areas with limited collection measures, it is likely that the leachate collection efficiency from these areas is low (i.e. the proportion of leachate generated that is subsequently collected). However, as this cannot be verified using onsite data at present, a 100% leachate collection efficiency was conservatively assumed from the existing landfilled areas.

6.5 Transfer station area

The existing transfer station at the WMF overlies existing waste, hence rainfall infiltrating the surface in this area would contribute to leachate generation. However, the concrete surface in this area is not able to be modelling using the infiltration modelling approach outlined in Section 5. As an alternative, an infiltration percentage of 3% was assumed for this area based on previous experience, and this was varied as part of the sensitivity analysis of the results.

6.6 Landfill staging

Based on feedback from Council, the existing landfill areas has been delineated into different areas based on the cover and capping status (refer Figure 6). The areas associated with this figure are summarised in Table 6.1 and are captured in each stage of the modelling, given they will remain consistent across the development of the South Cell. The proposed staging plans for the development of the South Cell are outlined in Figure 7 and 8, and summarised in Table 6.2, based on the design works being completed in parallel to this modelling. Leachate generation was modelled for each of these stages. The different scenarios were then reviewed to estimate the peak leachate generation volumes (based on the modelled parameters) across the life of the WMF and their impact on leachate management requirements.



Figure 6.1 Overview of existing cover and capping areas









NOTES:

FINAL SIDEWALL AND STEEP WALL GRADING SUBJECT TO OUTCOMES OF GEOTECHNICAL INVESTIGATION.
 ALL LOCATIONS ARE APPROXIMATE.



Table 6.1 Landfill staging – existing landfilled areas

| Stage | Description | Areas |
|--|-------------|---|
| Scenario 0 – Existing northern (existing layout and central areas | | Existing northern area (platform) = Intermediate cover area (platform) = 46,000 m² |
| | | - Existing northern area (batter) = Final capping Option 1 (batter) = $30,400 \text{ m}^2$ |
| | | Existing central area (northern batter) = Intermediate cover area (batter) = 20,700 m² |
| | | Existing central area (southern batter) = Final capping Option 1 (batter) = 20,300 m² |
| | | Existing central area (GO facility) = 6,300 m² |
| | | Existing central area (transfer station) = 11,800 m² |

Table 6.2 Landfill staging – South Cell

| Stage | Description | Areas |
|-----------------------|--|---|
| Scenario 1 | Western half of South Cell open | Open cell = 17,200 m² |
| Scenario 2 | Eastern half of South Cell open Western half of South Cell largely final capped with some remaining daily/interim cover | Open cell = 21,300 m² Daily cover area = 600 m² Interim cover area (platform) = 7,000 m² Final capping Option 2 (batter) = 10,200 m² |
| Scenario 3 (Final) | South Cell final capped | Final capping Option 2 (platform) = 15,900 m² Final capping Option 2 (batter) = 22,600 m² |

6.7 Storage and disposal capabilities

In line with current practices, it is proposed that stored leachate is discharged directly from the South Cell to the leachate storage dam and then onto the Woy Woy STP. As per Section 4.4, it is understood that there are no current restrictions on the leachate volumes or quality accepted by the treatment plant (SMEC, 2020).

The sewer disposal pipework would be upgraded alongside the South Cell development, with the final outcomes of this leachate water balance used to confirm the pipe size requirements.

In addition, the South Cell would be utilised for temporary emergency leachate level fluctuation where needed and this would be considered in subsequent design phases with regards to the instrumentation and controls for the pumping system. This would allow additional buffer prior to sewer disposal and reduce the potential risk for pond overflows.

6.8 Trigger action response

As outlined in Section 2, in extreme circumstances, the TARP within *Technical Report 1 - Soil and Water Impact Assessment* may require diversion of runoff from the GO facility and transfer station to the leachate management system. Specific to this leachate water balance, potential diversion of these flows to the leachate management system has been considered in terms of estimated leachate quantities, to confirm the system is adequate for this scenario. Quantitative estimates for these flows were developed as part of the sediment laden water estimates in the Soil and Water Impact Assessment, and utilised for the water balance results below.

6.9 Calibration with leachate flow data

As per Section 4.5, no onsite flow data was available at the time of preparing this report.

6.10 Results

6.10.1 Leachate generation estimates

The results of the leachate generation modelling can be found in Appendix B and are summarised in Table 6.3 (South Cell), Table 6.4 (whole of WMF) and Table 6.5 (whole of WMF plus GO facility and transfer station runoff) below.

| | | | | Estimated leachate generation for 10% AEP rainfall year | | | |
|---------|----------------------------------|--------------------------|------------------------|--|--------------------------|------------------------|--|
| | Average monthly (kL/month) | Peak month (kL/month) | Total for year (kL) | Average monthly (kL/month) | Peak month (kL/month) | Total for year (kL) | |
| Stage 1 | 1,730 | 4,590 | 20,760 | 2,500 | 6,670 | 29,970 | |
| Stage 2 | 2,350 | 6,070 | 28,140 | 3,480 | 9,330 | 41,740 | |
| Final | 40 | 200 | 510 | 70 | 280 | 840 | |

 Table 6.3
 Leachate generation modelling results (South Cell only)

Table 6.4

Leachate generation modelling results (whole of WMF)

| | | | | Estimated leachate generation for 10% AEP rainfall year | | | |
|---------|----------------------------------|--------------------------|------------------------|--|--------------------------|------------------------|--|
| | Average monthly (kL/month) | Peak month (kL/month) | Total for year (kL) | Average monthly (kL/month) | Peak month (kL/month) | Total for year (kL) | |
| Stage 1 | 4,040 | 9,300 | 48,510 | 6,560 | 17,430 | 78,770 | |
| Stage 2 | 4,510 | 10,530 | 54,130 | 7,390 | 19,760 | 88,670 | |
| Final | 2,190 | 4,620 | 26,250 | 3,970 | 10,710 | 47,650 | |

 Table 6.5
 Leachate generation modelling results (whole of WMF plus GO facility and transfer station runoff)

| | | | | Estimated leachate generation for 10% AEP rainfall year | | |
|---------|----------------------------------|--------------------------|------------------------|--|------------------------|---------|
| | Average monthly (kL/month) | Peak month (kL/month) | Total for year (kL) | Average monthly (kL/month) | Total for year (kL) | |
| Stage 1 | 5,150 | 10,410 | 67,150 | 10,310 | 21,170 | 105,330 |
| Stage 2 | 5,620 | 11,640 | 72,780 | 11,130 | 23,510 | 115,220 |
| Final | 3,300 | 5,730 | 44,890 | 7,710 | 14,460 | 74,200 |

6.10.2 Leachate disposal requirements

Given the limited storage capacity/buffer provided by the existing pond, leachate disposal requirements are estimated to be generally equivalent to the leachate generation estimates provided above. This could be reduced/buffered via use of the emergency in-cell storage during significant wet weather events, and this is discussed further below.

6.11 Discussion

The results provide estimates for leachate generation and subsequent disposal to sewer. As there is no specific limit for sewer disposal to the Woy Woy STP, no constraints have been identified in disposing of this leachate. In addition, as shown by the modelling the progressive capping and closure of the site will reduce leachate

generation and disposal requirements over time. The leachate collection and transfer infrastructure would be sized based on these estimates to provide adequate flow capacity within the leachate management system.

Based on the geometry of the South Cell, there is potential for temporary emergency storage of up to approximately 10 ML of leachate (7 ML in Stage 1 and 3 ML in Stage 2), should this be required during operations.

The following has been considered to address the limitations of the modelling:

- Calibration: As identified in Section 6.9, no leachate flow data was available to calibrate the model. As such, it is recommended that additional flow monitoring infrastructure (for both the South Cell and existing leachate pipework) be installed where possible as part of the South Cell construction. The collected data should then be used to calibrate, verify and/or update the leachate water balance within 1-2 years of the South Cell being commissioned, and every three years thereafter. In calibrating the model consideration should be given to developing and implementing a program to measure leachate levels in the existing filled areas and assess if any additional leachate volumes should be considered in the calibration exercise. This may also consider leachate seeps from the existing landfilled batters as an indicator of this issue.
- Groundwater inflow: As identified in Section 6.3, there is a potential for groundwater inflow to increase leachate generation within the unlined areas at the WMF, however this cannot be quantified with the available data. Qualitatively, WMF observations have suggested that the leachate management system for the existing landfilled areas was able to adequately manage leachate flows from these areas in recent years, including in 2022 during which significant rainfall and when there was a rise in the groundwater level. As discussed in the Soil and Water Impact Assessment, the monitoring data also suggests no leachate migration concerns at the groundwater monitoring locations. Hence, whilst not quantified, it is expected that the existing system can adequately address any additional leachate generated by groundwater inflow, and this can be quantified in future via the calibration works proposed above.

6.12 Model limitations

The HELP model is widely used (particularly in the USA) and is an industry accepted hydraulic modelling tool. It was developed for the United States Environmental Protection Agency to predict the hydraulic performance of differing landfill designs using site specific data.

The results of the HELP model tend to overestimate infiltration due to the use of daily instead of hourly data, which has the effect of reducing storm intensities and associated runoff quantities. There have been some concerns about using the HELP model in Australia, particularly in semi-arid to arid conditions, due to an under-estimation of evaporation rates in these climates. This under-estimation of evaporation rates tends to result in an overestimate of infiltration rates but for the purpose of design, some conservatism in the computed infiltration flows is appropriate.

7. Proposed leachate management measures

7.1 General

The following outlines the proposed leachate management measures at the WMF.

7.2 Minimisation

In line with current operations, leachate generation would be minimised through sound operating procedures including daily covering of wastes, the implementation of interim and final capping, effective surface water drainage and the use of landfill staging as parts of the cells are filled.

Filling of the South Cell is proposed to be separated into two stages, with the western half of the cell opened and filled first, followed by the eastern half of the cell, as outlined above in Table 6.2. These stages would limit the amount of "open cell" during operations, which would limit leachate generation during these phases.

Surface water drainage channels and diversions exist onsite to prevent the inflow of surface water into existing open cells. Surface water cut off drains and flow redirections are further outlined in Section 6.2.

7.3 Containment

The project would be fully lined across the cell footprint. The proposed liner profile options for the basal liner, sidewall liner, piggyback liner and steep wall liner for the project are described in the EIS. Each of the proposed liner profiles are designed in line with the NSW Landfill Guidelines and meet the design objectives.

7.4 Collection and transfer

The existing landfilled areas would continue to collect and transfer leachate in line with current operations. For the project, the proposed leachate collection and transfer system comprises (as described in the EIS):

- Perforated pipework to be laid at the base level of the project would be used to collect the generated leachate, which would be drained out by gravity.
- The collected drained leachate in a proposed sump within the extent of project would be extracted/transferred via a rising main to the upgraded sewer disposal network.

In addition, a contingency rising main would be installed alongside the rising main described above, to facilitate transfer of runoff from the GO facility and transfer station area if required based on the TARP implementation.

All of the proposed pipework would be sized based on the results of the leachate water balance described in this report.

7.5 Storage and disposal

For existing landfilled areas and the project, the existing leachate pond would be utilised for leachate storage prior disposal via sewer connection to the nearby Woy Woy STP. In addition, the project would be utilised for temporary emergency storage of leachate where needed and this would be considered in subsequent design phases with regards to the instrumentation and controls for the pumping system. This would allow additional buffer prior to sewer disposal and reduce the potential risk for pond overflows.

The sewer disposal pipework would be upgraded alongside the South Cell development, with the final outcomes of the leachate water balance used to confirm the pipe size requirements.

7.6 Monitoring

Alongside current compliance monitoring at the WMF, it is proposed that the following is implemented for the project:

- Leachate sump level monitoring via continuous monitoring measures (e.g. level switches) designed as part of the leachate collection and transfer system for the project.
- Yearly leachate quality monitoring in the sump in line with recommendations in the NSW Landfill Guidelines.
- Ongoing monitoring of the surrounding network of groundwater monitoring bores as outlined in *Technical* Report 1 - Soil and Water Impact Assessment.
- Ongoing monitoring of key surface water monitoring locations outlined in *Technical Report 1 Soil and Water Impact Assessment* to identify any potential leachate migration from the South Cell into the surface water at the site.

The design of the leachate management system would also include instrumentation and controls to determine when pumps are turned on and off based on leachate levels, and measure leachate flow transfer from the project to the Woy Woy STP. This flow measurement would be expanded to capture the leachate transfer pipework for the existing landfilled areas where possible.

7.7 Model calibration

The collected leachate flow data from the monitoring described in Section 7.6 should be used to calibrate, verify and/or update the leachate water balance within 1-2 years of the South Cell being commissioned, and every three years thereafter.

The calibration works will delineate the older existing areas from the South Cell to better assess their leachate generation with respect to impacts of items such as, capping deficiencies, groundwater inflow and leachate build-up.

8. Conclusions and recommendations

The report presents recommendations for the proposed leachate management measures for the South Cell, based on conclusions from the infiltration and leachate water balance modelling. These primarily consist of:

- Leachate minimisation via efficient staging of the South Cell operations, including progressive covering and capping and surface water diversion.
- Leachate containment via a suitably designed leachate barrier system for the South Cell.
- Leachate collection and transfer from the South Cell via an in-cell leachate collection system with leachate transferred to the upgraded sewer disposal network.
- Temporary leachate storage within the South Cell if needed, followed by disposal to the nearby Woy Woy STP.
- Ongoing monitoring of both leachate and water quality as well as quantity of leachate collected and transferred.
- Calibration of the leachate water balance presented in this report over time to determine if any changes to the leachate management system are warranted over time.

These recommendations should be incorporated into the detailed design of the South Cell and ongoing management during operation, closure and post-closure.

9. References

Bureau of Meteorology, 7 February 2023. Climate data for Mangrove Mountain AWS (BOM station number 061375)

Chase, Burke and Harvey Surveying, 2013. Capping Profile and the Five Year Capping Survey.

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GHD, 2023. South Cell at Woy Woy Waste Management Facility – Preliminary Design Report

NSW EPA, 2016. Environmental Guidelines: Solid Waste Landfills, Second edition, 2016

SILO, 7 February 2023. Weather data (<u>http://www.longpaddock.qld.gov.au/silo</u>) from SILO grid point of coordinates (-33.50, 151.30)

SMEC, 2020. Woy Woy Waste Management Facility - Development Strategy Report

Tetra Tech Coffey, 2022. Annual Environmental Monitoring Report, Woy Woy Waste Management Facility

US EPA, 1994. The Hydrologic Evaluation of Landfill Performance (HELP) Model

URS, 2006. Woy Woy Waste Management Facility Preliminary Closure Plan

URS, 2012. Landfill Management Plan (incorporating Pollution Incident Response Management Plan) – Woy Woy Waste Depot

Appendices

Appendix A HELP modelling outputs

| ♠ | | |
|---------|---|---------|
| ******* | *************************************** | ******* |
| ******* | *************************************** | <****** |
| ** | | ** |
| ** | | ** |
| ** | HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE | ** |
| ** | HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) | ** |
| ** | DEVELOPED BY ENVIRONMENTAL LABORATORY | ** |
| ** | USAE WATERWAYS EXPERIMENT STATION | ** |
| ** | FOR USEPA RISK REDUCTION ENGINEERING LABORATORY | ** |
| ** | | ** |
| ** | | ** |
| ******* | *************************************** | ****** |
| ******* | ****** | ****** |

| PRECIPITATION DATA FILE: | \WOY.D4 |
|----------------------------|------------|
| TEMPERATURE DATA FILE: | \WOY.D7 |
| SOLAR RADIATION DATA FILE: | \WOY.D13 |
| EVAPOTRANSPIRATION DATA: | \WOY10.D11 |
| SOIL AND DESIGN DATA FILE: | \DAILY.D10 |
| OUTPUT DATA FILE: | \DAILY.OUT |

TIME: 16: 1 DATE: 3/22/2023

TITLE: Daily Cover

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 14 THICKNESS 15.00 CM = POROSITY 0.4790 VOL/VOL = FIELD CAPACITY 0.3710 VOL/VOL = WILTING POINT 0.2510 VOL/VOL = INITIAL SOIL WATER CONTENT = 0.3058 VOL/VOL LAYER 2

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 18

| | NONDER 10 | | |
|---|------------------|--|---|
| = | 500.00 | СМ | |
| = | 0.6710 | VOL/VOL | |
| = | 0.2920 | VOL/VOL | |
| = | 0.0770 | VOL/VOL | |
| = | 0.2943 | VOL/VOL | |
| = | 0.10000009 | 5000E-02 | CM/SEC |
| | = = = = | = 0.6710 = 0.2920 = 0.0770 = 0.2943 | = 500.00 CM = 0.6710 VOL/VOL = 0.2920 VOL/VOL = 0.0770 VOL/VOL |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT SOIL DATA BASE USING SOIL TEXTURE #14 WITH BARE GROUND CONDITIONS, A SURFACE SLOPE OF 5.% AND A SLOPE LENGTH OF 50. METERS.

| SCS RUNOFF CURVE NUMBER | = | 96.50 | |
|------------------------------------|---|---------|----------|
| FRACTION OF AREA ALLOWING RUNOFF | = | 0.0 | PERCENT |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 1.0000 | HECTARES |
| EVAPORATIVE ZONE DEPTH | = | 10.0 | СМ |
| INITIAL WATER IN EVAPORATIVE ZONE | = | 2.661 | CM |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 4.790 | CM |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 2.510 | CM |
| INITIAL SNOW WATER | = | 0.000 | CM |
| INITIAL WATER IN LAYER MATERIALS | = | 151.756 | CM |
| TOTAL INITIAL WATER | = | 151.756 | CM |
| TOTAL SUBSURFACE INFLOW | = | 0.00 | MM/YR |

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM Woy Woy NSW

| STATION LATITUDE | = | -33.51 DEGR | EES |
|---------------------------------------|---|-------------|-----|
| MAXIMUM LEAF AREA INDEX | = | 0.00 | |
| START OF GROWING SEASON (JULIAN DATE) | = | 275 | |
| END OF GROWING SEASON (JULIAN DATE) | = | 91 | |

| EVAPORATIVE ZONE DEPTH | = | 10.0 | СМ |
|--------------------------|-----------------|-------|-----|
| AVERAGE ANNUAL WIND SPEE | :D = | 12.70 | KPH |
| AVERAGE 1ST QUARTER RELA | TIVE HUMIDITY = | 66.70 | % |
| AVERAGE 2ND QUARTER RELA | TIVE HUMIDITY = | 60.80 | % |
| AVERAGE 3RD QUARTER RELA | TIVE HUMIDITY = | 72.30 | % |
| AVERAGE 4TH QUARTER RELA | TIVE HUMIDITY = | 67.20 | % |

NOTE: PRECIPITATION DATA FOR

WAS ENTERED BY THE USER.

NOTE: TEMPERATURE DATA FOR

WAS ENTERED BY THE USER.

NOTE: SOLAR RADIATION DATA FOR

WAS ENTERED BY THE USER.

 MONTHLY TOTALS (MM) FOR YEAR 1952

 JAN/JUL FEB/AUG MAR/SEP APR/OCT MAY/NOV

 JUN/DEC

 PRECIPITATION
 46.4
 28.0
 228.0
 320.7
 45.6
 111.4

 RUNOFF
 0.00
 0.00
 0.00
 0.00
 0.00
 0.00

 EVAPOTRANSPIRATION
 20.00
 8.28
 44.38
 77.50
 40.98
 18.31
| PERCOLAT | ION/LEAKAGE THROUGH | 58.118 | 4.156 | 25.979 | 147.214 | 173.143 |
|----------|---------------------|--------|---------|---------|---------|---------|
| 97.160 | | | | | | |
| LAYER | 2 | 94.892 | 364.055 | 174.925 | 83.710 | 67.621 |
| 10.905 | | | | | | |

ANNUAL TOTALS FOR YEAR 1952

| | ММ | CU. METERS | PERCENT |
|-------------------------------|-------------|------------|---------|
| PRECIPITATION | 1701.50 | 17014.996 | 100.00 |
| RUNOFF | 0.000 | 0.000 | 0.00 |
| EVAPOTRANSPIRATION | 419.693 | 4196.929 | 24.67 |
| PERC./LEAKAGE THROUGH LAYER 2 | 1301.877080 | 13018.771 | 76.51 |
| CHANGE IN WATER STORAGE | -20.070 | -200.700 | -1.18 |
| SOIL WATER AT START OF YEAR | 1535.362 | 15353.617 | |
| SOIL WATER AT END OF YEAR | 1515.292 | 15152.917 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0004 | -0.004 | 0.00 |

MONTHLY TOTALS (MM) FOR YEAR 2008

JAN/JUL FEB/AUG MAR/SEP APR/OCT MAY/NOV JUN/DEC ----- ------ ------ ------ ------_ _ _ _ _ _ _ _ 106.7 257.2 46.3 166.1 13.5 164.3 PRECIPITATION 55.0 47.0 99.9 69.6 76.1 88.8 RUNOFF 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 37.19 68.39 38.87 56.22 10.08 52.19 EVAPOTRANSPIRATION 18.40 31.59 39.63 46.12 29.00 48.76 PERCOLATION/LEAKAGE THROUGH 81.598 100.253 104.554 60.328 105.198 63.022 LAYER 2 60.009 29.419 56.429 46.368 15.351 51.341

ANNUAL TOTALS FOR YEAR 2008

_

| | MM | CU. METERS | PERCENT |
|-------------------------------|------------|------------|---------|
| PRECIPITATION | 1190.50 | 11904.997 | 100.00 |
| RUNOFF | 0.000 | 0.000 | 0.00 |
| EVAPOTRANSPIRATION | 476.452 | 4764.515 | 40.02 |
| PERC./LEAKAGE THROUGH LAYER 2 | 773.870605 | 7738.707 | 65.00 |
| CHANGE IN WATER STORAGE | -59.822 | -598.221 | -5.02 |
| SOIL WATER AT START OF YEAR | 1584.238 | 15842.376 | |
| SOIL WATER AT END OF YEAR | 1524.415 | 15244.154 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |

| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
|-----------------------------|---------|--------|------|
| ANNUAL WATER BUDGET BALANCE | -0.0003 | -0.003 | 0.00 |

AVERAGE MONTHLY VALUES (MM) FOR YEARS 1923 THROUGH 2022

| PRECIPITATION | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|--------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| TOTALS | 108.32 70.25 | 125.65 70.88 | 140.77 62.27 | 121.45 75.55 | 100.17 86.71 | 120.21 91.16 |
| STD. DEVIATIONS | 74.48 65.33 | 85.28 74.25 | 94.50 50.54 | 101.89 56.69 | 75.37 62.89 | |
| RUNOFF | | | | | | |
| TOTALS | 0.000 0.000 | 0.000 0.000 | 0.000 0.000 | 0.000 0.000 | 0.000 0.000 | 0.000 0.000 |
| STD. DEVIATIONS | 0.000 0.000 | 0.000 0.000 | 0.000 0.000 | 0.000 0.000 | 0.000 0.000 | 0.000 0.000 |
| EVAPOTRANSPIRATION | | | | | | |
| TOTALS | 48.096 26.789 | 47.936 27.412 | 52.254 29.274 | 44.928 37.696 | 36.001 43.342 | |
| STD. DEVIATIONS | 21.313 12.984 | 24.259 16.433 | 24.029 16.823 | 22.217 18.777 | 16.023 22.983 | 14.990 24.861 |

PERCOLATION/LEAKAGE THROUGH LAYER 2

| TOTALS | | 75.4286 41.7436 | | |
|-----------------|------|--------------------|------|--|
| STD. DEVIATIONS | | 47.0601 41.4941 | | |

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1923 THROUGH 2022

| | |
|------|------|

| | MM | 4 | CU. METERS | PERCENT |
|--|-----------|-------------|------------|----------|
| PRECIPITATION | 1173.39 | (283.704) | 11733.9 | 100.00 |
| RUNOFF | 0.000 | (0.0000) | 0.00 | 0.000 |
| EVAPOTRANSPIRATION | 473.354 | (89.2795) | 4733.54 | 40.341 |
| PERCOLATION/LEAKAGE THROUGH LAYER 2 | 700.13257 | (232.32204) | 7001.326 | 59.66773 |
| CHANGE IN WATER STORAGE | -0.101 | (2.3479) | -1.01 | -0.009 |

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PEAK DAILY VALUES FOR YEARS 1923 THROUGH 2022

| | | (MM) | (CU. METERS) |
|-----------------------------------|---|-----------|--------------|
| PRECIPITATION | | 150.40 | 1504.000 |
| RUNOFF | | 0.000 | 0.0000 |
| PERCOLATION/LEAKAGE THROUGH LAYER | 2 | 24.715059 | 247.15059 |
| SNOW WATER | | 0.00 | 0.0000 |
| | | | |

MAXIMUM VEG. SOIL WATER (VOL/VOL)

0.4790

MINIMUM VEG. SOIL WATER (VOL/VOL) 0.2510

| FINAL WATER | STORAGE AT END | D OF YEAR 2022 |
|-------------|----------------|----------------|
| LAYER | (CM) | (VOL/VOL) |
| 1 | 4.7480 | 0.3165 |
| 2 | 146.0000 | 0.2920 |
| SNOW WATER | 0.000 | |

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| ******* | *************************************** | <******* |
| ** | | ** |
| ** | | ** |
| ** | HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE | ** |
| ** | HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) | ** |
| ** | DEVELOPED BY ENVIRONMENTAL LABORATORY | ** |
| ** | USAE WATERWAYS EXPERIMENT STATION | ** |
| ** | FOR USEPA RISK REDUCTION ENGINEERING LABORATORY | ** |
| ** | | ** |
| ** | | ** |
| ******* | *************************************** | ****** |
| ******** | *************************************** | ****** |

| PRECIPITATION DATA FILE: | \WOY.D4 |
|----------------------------|--------------|
| TEMPERATURE DATA FILE: | \WOY.D7 |
| SOLAR RADIATION DATA FILE: | \WOY.D13 |
| EVAPOTRANSPIRATION DATA: | \WOY20.D11 |
| SOIL AND DESIGN DATA FILE: | \INTPLAT.D10 |
| OUTPUT DATA FILE: | \INTPLAT.OUT |

TIME: 16: 6 DATE: 3/22/2023

TITLE: Intermediate Cover - PLATFORM

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 14 THICKNESS 30.00 CM = POROSITY 0.4790 VOL/VOL = FIELD CAPACITY 0.3710 VOL/VOL = WILTING POINT 0.2510 VOL/VOL = INITIAL SOIL WATER CONTENT = 0.3462 VOL/VOL LAYER 2

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 18

| | | NONDER 10 | | |
|----------------------------|-----|-------------|--------------|----|
| THICKNESS | = | 500.00 (| CM | |
| POROSITY | = | 0.6710 \ | /OL/VOL | |
| FIELD CAPACITY | = | 0.2920 \ | /OL/VOL | |
| WILTING POINT | = | 0.0770 \ | /OL/VOL | |
| INITIAL SOIL WATER CONTENT | - = | 0.2920 \ | /OL/VOL | |
| EFFECTIVE SAT. HYD. COND. | = | 0.100000050 | 000E-02 CM/S | EC |
| | | | | |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT SOIL DATA BASE USING SOIL TEXTURE #14 WITH BARE GROUND CONDITIONS, A SURFACE SLOPE OF 5.% AND A SLOPE LENGTH OF 225. METERS.

| SCS RUNOFF CURVE NUMBER | = | 96.30 | |
|------------------------------------|---|---------|----------|
| FRACTION OF AREA ALLOWING RUNOFF | = | 50.0 | PERCENT |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 1.0000 | HECTARES |
| EVAPORATIVE ZONE DEPTH | = | 20.0 | СМ |
| INITIAL WATER IN EVAPORATIVE ZONE | = | 6.348 | СМ |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 9.580 | СМ |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 5.020 | СМ |
| INITIAL SNOW WATER | = | 0.000 | CM |
| INITIAL WATER IN LAYER MATERIALS | = | 156.382 | СМ |
| TOTAL INITIAL WATER | = | 156.382 | CM |
| TOTAL SUBSURFACE INFLOW | = | 0.00 | MM/YR |

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM Woy Woy NSW

STATION LATITUDE= -33.51 DEGREESMAXIMUM LEAF AREA INDEX= 0.00START OF GROWING SEASON (JULIAN DATE)= 275END OF GROWING SEASON (JULIAN DATE)= 91

| EVAPORATIVE 2 | ZONE DEF | PTH | | = | 20.0 | CM |
|---------------|----------|----------|----------|---|-------|-----|
| AVERAGE ANNU | AL WIND | SPEED | | = | 12.70 | KPH |
| AVERAGE 1ST | QUARTER | RELATIVE | HUMIDITY | = | 66.70 | % |
| AVERAGE 2ND | QUARTER | RELATIVE | HUMIDITY | = | 60.80 | % |
| AVERAGE 3RD | QUARTER | RELATIVE | HUMIDITY | = | 72.30 | % |
| AVERAGE 4TH | QUARTER | RELATIVE | HUMIDITY | = | 67.20 | % |

NOTE: PRECIPITATION DATA FOR

WAS ENTERED BY THE USER.

NOTE: TEMPERATURE DATA FOR

WAS ENTERED BY THE USER.

NOTE: SOLAR RADIATION DATA FOR

WAS ENTERED BY THE USER.

MONTHLY TOTALS (MM) FOR YEAR 1952

 JAN/JUL FEB/AUG MAR/SEP APR/OCT MAY/NOV

 JUN/DEC

 PRECIPITATION

 46.4
 28.0
 228.0
 320.7
 45.6
 111.4

 317.4
 371.3
 24.4
 115.1
 43.1
 50.1

 RUNOFF
 9.09
 1.25
 79.29
 88.24
 2.59
 35.00

 131.02
 132.73
 0.56
 19.40
 1.68
 1.77

 EVAPOTRANSPIRATION
 34.81
 7.54
 62.10
 89.65
 65.22
 32.58

 18.72
 73.70
 9.10
 83.25
 34.11
 38.06

| PERCOLAT | ION/LEAKAGE THROUGH | 3.019 | 0.000 | 18.489 | 67.669 1 | 03.775 |
|----------|---------------------|--------|---------|---------|----------|--------|
| 50.065 | | | | | | |
| LAYER | 2 | 32.069 | 144.187 | 140.892 | 65.679 | 3.416 |
| 0.000 | | | | | | |

ANNUAL TOTALS FOR YEAR 1952

| | MM | CU. METERS | PERCENT |
|-------------------------------|------------|------------|---------|
| PRECIPITATION | 1701.50 | 17014.996 | 100.00 |
| RUNOFF | 502.611 | 5026.106 | 29.54 |
| EVAPOTRANSPIRATION | 548.866 | 5488.658 | 32.26 |
| PERC./LEAKAGE THROUGH LAYER 2 | 629.260498 | 6292.605 | 36.98 |
| CHANGE IN WATER STORAGE | 20.763 | 207.634 | 1.22 |
| SOIL WATER AT START OF YEAR | 1547.804 | 15478.035 | |
| SOIL WATER AT END OF YEAR | 1568.567 | 15685.669 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0006 | -0.006 | 0.00 |
| | | | |

MONTHLY TOTALS (MM) FOR YEAR 2008

JAN/JUL FEB/AUG MAR/SEP APR/OCT MAY/NOV JUN/DEC ----- ------ ------ ------_ _ _ _ _ _ _ _ 106.7257.246.3166.113.5164.355.047.099.969.676.188.8 PRECIPITATION RUNOFF 21.10 65.90 4.74 38.74 0.11 39.94 6.63 3.70 28.74 5.33 10.84 18.51 EVAPOTRANSPIRATION 50.67 87.04 61.51 74.15 20.21 63.82 21.52 47.23 49.62 55.00 47.01 71.21 36.661 57.084 48.406 13.504 33.313 PERCOLATION/LEAKAGE THROUGH 40.822 24.256 4.415 38.286 4.881 6.987 LAYER 2 13.627

ANNUAL TOTALS FOR YEAR 2008

| | ММ | CU. METERS | PERCENT |
|-------------------------------|------------|------------|---------|
| PRECIPITATION | 1190.50 | 11904.997 | 100.00 |
| RUNOFF | 244.280 | 2442.800 | 20.52 |
| EVAPOTRANSPIRATION | 648.982 | 6489.815 | 54.51 |
| PERC./LEAKAGE THROUGH LAYER 2 | 322.244476 | 3222.445 | 27.07 |
| CHANGE IN WATER STORAGE | -25.006 | -250.061 | -2.10 |
| SOIL WATER AT START OF YEAR | 1575.933 | 15759.326 | |
| SOIL WATER AT END OF YEAR | 1550.927 | 15509.266 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0002 | -0.002 | 0.00 |

AVERAGE MONTHLY VALUES (MM) FOR YEARS 1923 THROUGH 2022

| | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------------|--------------------|--------------------|------------------|------------------|------------------|------------------|
| PRECIPITATION | | | | | | |
| TOTALS | 108.32 70.25 | 125.65 70.88 | 140.77 62.27 | 121.45 75.55 | 100.17 86.71 | 120.21 91.16 |
| STD. DEVIATIONS | 74.48 65.33 | 85.28 74.25 | 94.50 50.54 | 101.89 56.69 | 75.37 62.89 | 96.67 65.51 |
| RUNOFF | | | | | | |
| TOTALS | 22.188 14.370 | 28.572 14.737 | 32.459 10.559 | 28.221 13.103 | 22.069 15.394 | 28.308 16.865 |
| STD. DEVIATIONS | 24.942 22.439 | 26.988 25.375 | 31.337 14.429 | 34.740 17.068 | 24.563 19.838 | 32.528 20.367 |
| EVAPOTRANSPIRATION | | | | | | |
| TOTALS | 62.491 36.001 | 62.324 36.495 | 66.097 37.771 | 58.604 49.112 | 46.569 53.549 | 45.685 55.816 |
| STD. DEVIATIONS | 27.143 15.758 | 30.676 21.217 | 28.595 22.203 | 26.507 24.703 | 19.197 29.914 | 17.700 32.323 |
| PERCOLATION/LEAKAGE T | HROUGH LAY | ER 2 | | | | |
| TOTALS | 16.3613 39.3497 | | | | | |
| STD. DEVIATIONS | 18.2482 34.3125 | 22.1719 31.3496 | | | | |

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1923 THROUGH 2022

| - | | | | | |
|---|--|-----------|-------------|------------|----------|
| | | MM | 1 | CU. METERS | PERCENT |
| | PRECIPITATION | 1173.39 | (283.704) | 11733.9 | 100.00 |
| | RUNOFF | 246.845 | (88.7719) | 2468.45 | 21.037 |
| | EVAPOTRANSPIRATION | 610.513 | (109.0491) | 6105.13 | 52.030 |
| | PERCOLATION/LEAKAGE THROUGH LAYER 2 | 316.07736 | (123.38899) | 3160.774 | 26.93721 |
| | CHANGE IN WATER STORAGE | -0.050 | (1.1163) | -0.50 | -0.004 |

PEAK DAILY VALUES FOR YEARS 1923 THROUGH 2022

| | (MM) | (CU. METERS) |
|-------------------------------------|----------|--------------|
| PRECIPITATION | 150.40 | 1504.000 |
| RUNOFF | 70.107 | 701.0656 |
| PERCOLATION/LEAKAGE THROUGH LAYER 2 | 9.531699 | 95.31699 |
| SNOW WATER | 0.00 | 0.0000 |
| MAXIMUM VEG. SOIL WATER (VOL/VOL) | 0 | .4520 |
| MINIMUM VEG. SOIL WATER (VOL/VOL) | 0 | .2510 |

| FINAL WATER | STORAGE AT EN | O OF YEAR 2022 | |
|-------------|---------------|----------------|--|
| LAYER | (CM) | (VOL/VOL) | |
| 1 | 10.0084 | 0.3336 | |
| 2 | 145.8777 | 0.2918 | |
| SNOW WATER | 0.000 | | |

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|----------|---|---------|
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| ******** | *************************************** | ****** |
| ** | | ** |
| ** | | ** |
| ** | HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE | ** |
| ** | HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) | ** |
| ** | DEVELOPED BY ENVIRONMENTAL LABORATORY | ** |
| ** | USAE WATERWAYS EXPERIMENT STATION | ** |
| ** | FOR USEPA RISK REDUCTION ENGINEERING LABORATORY | ** |
| ** | | ** |
| ** | | ** |
| ******* | *************************************** | ******* |
| ******* | *************************************** | ****** |

| PRECIPITATION DATA FILE: | \WOY.D4 |
|----------------------------|-------------|
| TEMPERATURE DATA FILE: | \WOY.D7 |
| SOLAR RADIATION DATA FILE: | \WOY.D13 |
| EVAPOTRANSPIRATION DATA: | \WOY20.D11 |
| SOIL AND DESIGN DATA FILE: | \INTBAT.D10 |
| OUTPUT DATA FILE: | \INTBAT.OUT |

TIME: 16:15 DATE: 3/22/2023

TITLE: Intermediate Cover - BATTER

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 14 THICKNESS 30.00 CM = POROSITY 0.4790 VOL/VOL = FIELD CAPACITY 0.3710 VOL/VOL = WILTING POINT 0.2510 VOL/VOL = INITIAL SOIL WATER CONTENT = 0.3518 VOL/VOL LAYER 2

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 18

| OILE | NOUPER TO | | |
|------|------------------|--|---|
| = | 500.00 | СМ | |
| = | 0.6710 | VOL/VOL | |
| = | 0.2920 | VOL/VOL | |
| = | 0.0770 | VOL/VOL | |
| = | 0.2919 | VOL/VOL | |
| = | 0.10000005 | 000E-02 | CM/SEC |
| | = = = = | = 0.6710 = 0.2920 = 0.0770 = 0.2919 | = 500.00 CM = 0.6710 VOL/VOL = 0.2920 VOL/VOL = 0.0770 VOL/VOL |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT SOIL DATA BASE USING SOIL TEXTURE #14 WITH BARE GROUND CONDITIONS, A SURFACE SLOPE OF 15.% AND A SLOPE LENGTH OF 90. METERS.

| SCS RUNOFF CURVE NUMBER | = | 96.50 | |
|------------------------------------|---|---------|----------|
| FRACTION OF AREA ALLOWING RUNOFF | = | 50.0 | PERCENT |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 1.0000 | HECTARES |
| EVAPORATIVE ZONE DEPTH | = | 20.0 | СМ |
| INITIAL WATER IN EVAPORATIVE ZONE | = | 6.649 | СМ |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 9.580 | СМ |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 5.020 | СМ |
| INITIAL SNOW WATER | = | 0.000 | CM |
| INITIAL WATER IN LAYER MATERIALS | = | 156.510 | СМ |
| TOTAL INITIAL WATER | = | 156.510 | СМ |
| TOTAL SUBSURFACE INFLOW | = | 0.00 | MM/YR |

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM Woy Woy NSW

STATION LATITUDE= -33.51 DEGREESMAXIMUM LEAF AREA INDEX= 0.00START OF GROWING SEASON (JULIAN DATE)= 275END OF GROWING SEASON (JULIAN DATE)= 91

| EVAPORATIVE 2 | ZONE DEF | PTH | | = | 20.0 | CM |
|---------------|----------|----------|----------|---|-------|-----|
| AVERAGE ANNU | AL WIND | SPEED | | = | 12.70 | KPH |
| AVERAGE 1ST | QUARTER | RELATIVE | HUMIDITY | = | 66.70 | % |
| AVERAGE 2ND | QUARTER | RELATIVE | HUMIDITY | = | 60.80 | % |
| AVERAGE 3RD | QUARTER | RELATIVE | HUMIDITY | = | 72.30 | % |
| AVERAGE 4TH | QUARTER | RELATIVE | HUMIDITY | = | 67.20 | % |

NOTE: PRECIPITATION DATA FOR

WAS ENTERED BY THE USER.

NOTE: TEMPERATURE DATA FOR

WAS ENTERED BY THE USER.

NOTE: SOLAR RADIATION DATA FOR

WAS ENTERED BY THE USER.

MONTHLY TOTALS (MM) FOR YEAR 1952

 JAN/JUL FEB/AUG MAR/SEP APR/OCT MAY/NOV

 JUN/DEC

 PRECIPITATION

 46.4
 28.0
 228.0
 320.7
 45.6
 111.4

 317.4
 371.3
 24.4
 115.1
 43.1
 50.1

 RUNOFF
 9.50
 1.40
 80.35
 90.69
 2.82
 35.67

 I31.86
 134.73
 0.65
 20.43
 1.88
 1.79

 EVAPOTRANSPIRATION
 34.56
 7.54
 62.12
 89.15
 64.56
 32.54

 18.72
 73.43
 9.12
 82.96
 26.93
 41.71

| PERCOLAT | ION/LEAKAGE THROUGH | 2.163 | 0.000 | 18.012 | 67.704 1 | .02.974 |
|----------|---------------------|--------|---------|---------|----------|---------|
| 49.302 | | | | | | |
| LAYER | 2 | 30.897 | 142.247 | 140.310 | 63.460 | 2.165 |
| 5.181 | | | | | | |

ANNUAL TOTALS FOR YEAR 1952

| | MM | CU. METERS | PERCENT |
|-------------------------------|------------|------------|---------|
| PRECIPITATION | 1701.50 | 17014.996 | 100.00 |
| RUNOFF | 511.765 | 5117.648 | 30.08 |
| EVAPOTRANSPIRATION | 543.354 | 5433.542 | 31.93 |
| PERC./LEAKAGE THROUGH LAYER 2 | 624.414551 | 6244.146 | 36.70 |
| CHANGE IN WATER STORAGE | 21.967 | 219.666 | 1.29 |
| SOIL WATER AT START OF YEAR | 1546.972 | 15469.717 | |
| SOIL WATER AT END OF YEAR | 1568.938 | 15689.382 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| NOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0006 | -0.006 | 0.00 |

MONTHLY TOTALS (MM) FOR YEAR 2008

| JUN/DEC | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | |
|------------------------------------|----------------|----------------|----------------|----------------|----------------|----------------|
| | | | | | | |
| PRECIPITATION | 106.7 55.0 | 257.2 47.0 | 46.3 99.9 | 166.1 69.6 | 13.5 76.1 | 164.3 88.8 |
| RUNOFF | 21.97 6.96 | 66.09 4.01 | 5.11 29.42 | 39.81 5.74 | 0.14 11.56 | 41.10 19.00 |
| EVAPOTRANSPIRATION | 50.63 21.82 | 84.11 46.22 | 60.96 50.44 | 71.32 53.62 | 20.40 47.83 | 63.39 69.84 |
| PERCOLATION/LEAKAGE THROUGH 42.172 | 27.822 | 56.560 | 53.201 | 14.253 | 33.459 | |
| LAYER 2 14.217 | 21.770 | 4.427 | 37.204 | 6.428 | 5.179 | |

ANNUAL TOTALS FOR YEAR 2008

| | ММ | CU. METERS | PERCENT |
|-------------------------------|------------|------------|---------|
| PRECIPITATION | 1190.50 | 11904.997 | 100.00 |
| RUNOFF | 250.925 | 2509.248 | 21.08 |
| EVAPOTRANSPIRATION | 640.575 | 6405.747 | 53.81 |
| PERC./LEAKAGE THROUGH LAYER 2 | 316.692047 | 3166.920 | 26.60 |
| CHANGE IN WATER STORAGE | -17.692 | -176.917 | -1.49 |
| SOIL WATER AT START OF YEAR | 1568.599 | 15685.985 | |
| SOIL WATER AT END OF YEAR | 1550.907 | 15509.067 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |

| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
|-----------------------------|---------|--------|------|
| ANNUAL WATER BUDGET BALANCE | -0.0001 | -0.001 | 0.00 |

AVERAGE MONTHLY VALUES (MM) FOR YEARS 1923 THROUGH 2022

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| | |
|------|------|
| | |

| | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC | |
|-------------------------------------|------------------|------------------|-----------------|-----------------|------------------|-----------------|--|
| PRECIPITATION | | | | | | | |
| TOTALS | 108.32 70.25 | 125.65 70.88 | 140.77 62.27 | 121.45 75.55 | 100.17 86.71 | 120.21 91.16 | |
| STD. DEVIATIONS | 74.48 65.33 | 85.28 74.25 | | 101.89 56.69 | | | |
| RUNOFF | | | | | | | |
| TOTALS | 22.965 14.850 | 29.434 15.168 | | | 22.719 15.943 | | |
| STD. DEVIATIONS | 25.434 22.774 | 27.513 25.806 | | | 25.026 20.135 | | |
| EVAPOTRANSPIRATION | | | | | | | |
| TOTALS | 62.341 35.931 | 61.625 36.465 | | | | | |
| STD. DEVIATIONS | 27.095 15.814 | 30.797 21.319 | | | | | |
| PERCOLATION/LEAKAGE THROUGH LAYER 2 | | | | | | | |

TOTALS 15.9369 23.8075 35.6081 35.5866 35.2203 33.4624

| | 38.6760 | 23.7714 | 17.6965 | 17.0045 | 15.8720 | 17.6193 |
|-----------------|---------|---------|---------|---------|--------------------|---------|
| STD. DEVIATIONS | | | | | 34.5039 18.7634 | |

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1923 THROUGH 2022

| | M | 4 | CU. METERS | PERCENT |
|--|-----------|-------------|------------|----------|
| PRECIPITATION | 1173.39 | (283.704) | 11733.9 | 100.00 |
| RUNOFF | 254.688 | (90.4030) | 2546.88 | 21.705 |
| EVAPOTRANSPIRATION | 608.491 | (108.6803) | 6084.91 | 51.858 |
| PERCOLATION/LEAKAGE THROUGH LAYER 2 | 310.26135 | (121.85497) | 3102.614 | 26.44155 |
| CHANGE IN WATER STORAGE | -0.054 | (1.1207) | -0.54 | -0.005 |

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PEAK DAILY VALUES FOR YEARS 1923 THROUGH 2022

| | (MM) | (CU. METERS) |
|-------------------------------------|----------|--------------|
| PRECIPITATION | 150.40 | 1504.000 |
| RUNOFF | 70.329 | 703.2940 |
| PERCOLATION/LEAKAGE THROUGH LAYER 2 | 9.418694 | 94.18694 |
| SNOW WATER | 0.00 | 0.0000 |
| | | |
| MAXIMUM VEG. SOIL WATER (VOL/VOL) | 0. | 4526 |
| MINIMUM VEG. SOIL WATER (VOL/VOL) | 0. | 2510 |

♠ FINAL WATER STORAGE AT END OF YEAR 2022 _____ (CM) LAYER (VOL/VOL) -------------10.0051 1 0.3335 145.9629 2 0.2919 SNOW WATER 0.000

| ♠ | | |
|----------|---|---------|
| ******** | *************************************** | ******* |
| ******* | *************************************** | ****** |
| ** | | ** |
| ** | | ** |
| ** | HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE | ** |
| ** | HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) | ** |
| ** | DEVELOPED BY ENVIRONMENTAL LABORATORY | ** |
| ** | USAE WATERWAYS EXPERIMENT STATION | ** |
| ** | FOR USEPA RISK REDUCTION ENGINEERING LABORATORY | ** |
| ** | | ** |
| ** | | ** |
| ******** | *************************************** | ******* |
| ******* | *************************************** | ******* |

| PRECIPITATION DATA FILE: | \WOY.D4 |
|----------------------------|---------------|
| TEMPERATURE DATA FILE: | \WOY.D7 |
| SOLAR RADIATION DATA FILE: | \WOY.D13 |
| EVAPOTRANSPIRATION DATA: | \WOY15.D11 |
| SOIL AND DESIGN DATA FILE: | \FIN1PLAT.D10 |
| OUTPUT DATA FILE: | \FIN1PLAT.OUT |

TIME: 16:22 DATE: 3/22/2023

TITLE: Final Cap Option 1 - PLATFORM

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 8 THICKNESS 15.00 CM = POROSITY 0.4630 VOL/VOL = FIELD CAPACITY 0.2320 VOL/VOL = WILTING POINT 0.1160 VOL/VOL = INITIAL SOIL WATER CONTENT = 0.1348 VOL/VOL EFFECTIVE SAT. HYD. COND. = 0.369999994000E-03 CM/SEC NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 1.80 FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2

TYPE 3 - BARRIER SOIL LINER
MATERIAL TEXTURE NUMBER 0THICKNESS=90.00 CMPOROSITY=0.4270 VOL/VOLFIELD CAPACITY=0.4180 VOL/VOLWILTING POINT=0.3670 VOL/VOLINITIAL SOIL WATER CONTENT=0.4270 VOL/VOLEFFECTIVE SAT. HYD. COND.=0.999999997000E-06 CM/SEC

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 14

| THICKNESS | = | 30.00 CM |
|----------------------------|---|---------------------------|
| POROSITY | = | 0.4790 VOL/VOL |
| FIELD CAPACITY | = | 0.3710 VOL/VOL |
| WILTING POINT | = | 0.2510 VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.3710 VOL/VOL |
| EFFECTIVE SAT. HYD. COND. | = | 0.249999994000E-04 CM/SEC |

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 18

| MATE | NIAL ILVIONE | NUMBER 10 | |
|--------------------|--------------|------------|-----------------|
| THICKNESS | = | 500.00 | CM |
| POROSITY | = | 0.6710 | VOL/VOL |
| FIELD CAPACITY | = | 0.2920 | VOL/VOL |
| WILTING POINT | = | 0.0770 | VOL/VOL |
| INITIAL SOIL WATER | CONTENT = | 0.2919 | VOL/VOL |
| EFFECTIVE SAT. HYD | . COND. = | 0.10000009 | 5000E-02 CM/SEC |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT SOIL DATA BASE USING SOIL TEXTURE # 8 WITH A POOR STAND OF GRASS, A SURFACE SLOPE OF 5.% AND A SLOPE LENGTH OF 225. METERS.

| SCS RUNOFF CURVE NUMBER | = | 85.50 | |
|------------------------------------|---|---------|----------|
| FRACTION OF AREA ALLOWING RUNOFF | = | 75.0 | PERCENT |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 1.0000 | HECTARES |
| EVAPORATIVE ZONE DEPTH | = | 15.0 | СМ |
| INITIAL WATER IN EVAPORATIVE ZONE | = | 2.023 | CM |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 6.945 | CM |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 1.740 | CM |
| INITIAL SNOW WATER | = | 0.000 | CM |
| INITIAL WATER IN LAYER MATERIALS | = | 197.542 | CM |
| TOTAL INITIAL WATER | = | 197.542 | CM |
| TOTAL SUBSURFACE INFLOW | = | 0.00 | MM/YR |

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM Woy Woy NSW

| STATION LATITUDE | = | -33.51 | DEGREES |
|---------------------------------------|---|--------|---------|
| MAXIMUM LEAF AREA INDEX | = | 1.00 | |
| START OF GROWING SEASON (JULIAN DATE) | = | 275 | |
| END OF GROWING SEASON (JULIAN DATE) | = | 91 | |
| EVAPORATIVE ZONE DEPTH | = | 15.0 | CM |
| AVERAGE ANNUAL WIND SPEED | = | 12.70 | KPH |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 66.70 | % |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 60.80 | % |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 72.30 | % |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 67.20 | % |

NOTE: PRECIPITATION DATA FOR

WAS ENTERED BY THE USER.

NOTE: TEMPERATURE DATA FOR

WAS ENTERED BY THE USER.

NOTE: SOLAR RADIATION DATA FOR

WAS ENTERED BY THE USER.

| *************************************** | | | | | | | | | |
|---|-----------|----------|----------------|---------|---------|---------------|--|--|--|
| MONTHLY TO | TALS (MM) |) FOR YE | AR 1952 | | | | | | |
| | | | | | | | | | |
| | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | | | | |
| JUN/DEC | | | | | | | | | |
| | | | | | | | | | |
| PRECIPITATION | | | 228.0 24.4 | | | 111.4 50.1 | | | |
| RUNOFF | | 0.00 | 116.76 | | | 46.60 | | | |
| | 244.02 | 305.63 | 0.00 | 2.65 | 0.00 | 0.00 | | | |
| EVAPOTRANSPIRATION | | | 82.53 23.15 | | | | | | |
| PERCOLATION/LEAKAGE THROUGH | 4.839 | 0.000 | 7.985 | 29.488 | 28.818 | | | | |
| 16.587 LAYER 2 | 12.882 | 30.243 | 2.234 | 15.130 | 0.879 | | | | |
| 0.000 | 0 055 | | | | | | | | |
| PERCOLATION/LEAKAGE THROUGH 16.502 | 8.055 | 0.000 | 0.000 | 24.534 | 29.582 | | | | |
| LAYER 4 0.000 | 18.019 | 24.911 | 15.030 | 7.299 | 8.173 | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| MONTHLY SU | MMARIES I | FOR DAIL | Y HEADS | (CM) | | | | | |
| | | | | | | | | | |
| AVERAGE DAILY HEAD ON | | | | | 6.837 | | | | |
| TOP OF LAYER 2 | 3.369 | 11.623 | 0.156 | 3.664 | 0.052 | 0.000 | | | |
| STD. DEVIATION OF DAILY | 1.619 | 0.000 | 5.161 | 3.300 | 2.810 | 5.488 | | | |

HEAD ON TOP OF LAYER 2 5.384 3.520 0.545 4.365 0.280 0.000

ANNUAL TOTALS FOR YEAR 1952

| | MM | CU. METERS | PERCENT |
|-------------------------------|------------|------------|---------|
| PRECIPITATION | 1701.50 | 17014.996 | 100.00 |
| RUNOFF | 904.351 | 9043.513 | 53.15 |
| EVAPOTRANSPIRATION | 638.341 | 6383.414 | 37.52 |
| PERC./LEAKAGE THROUGH LAYER 2 | 149.084061 | 1490.841 | 8.76 |
| AVG. HEAD ON TOP OF LAYER 2 | 39.0223 | | |
| PERC./LEAKAGE THROUGH LAYER 4 | 152.103912 | 1521.039 | 8.94 |
| CHANGE IN WATER STORAGE | 6.703 | 67.035 | 0.39 |
| SOIL WATER AT START OF YEAR | 1975.953 | 19759.529 | |
| SOIL WATER AT END OF YEAR | 1982.656 | 19826.564 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0005 | -0.005 | 0.00 |
| | | | |

MONTHLY TOTALS (MM) FOR YEAR 2008

| | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | | |
|---|-----------|---------------|----------------|---------------|---------|----------------|--|
| JUN/DEC | | | | | | | |
| | | | | | | | |
| PRECIPITATION | | 257.2 47.0 | 46.3 99.9 | 166.1 69.6 | | 164.3 88.8 | |
| RUNOFF | | | 0.00 37.13 | | | 68.75 3.41 | |
| EVAPOTRANSPIRATION | | | 72.64 66.48 | | | 52.58 95.83 | |
| PERCOLATION/LEAKAGE THROUGH 26.150 | 10.881 | 18.836 | 3.791 | 20.700 | 9.564 | | |
| LAYER 2 8.811 | 13.020 | 11.383 | 13.652 | 2.036 | 0.628 | | |
| PERCOLATION/LEAKAGE THROUGH | 7.735 | 21.235 | 10.760 | 7.472 | 20.906 | | |
| 15.627 LAYER 4 6.276 | 18.067 | 15.487 | 12.440 | 6.255 | 0.604 | | |
| MONTHLY SUMMARIES FOR DAILY HEADS (CM) | | | | | | | |
| AVERAGE DAILY HEAD ON TOP OF LAYER 2 | | | 0.403 3.905 | | | | |
| STD. DEVIATION OF DAILY HEAD ON TOP OF LAYER 2 | | | 1.013 5.145 | | | | |
| ********** | ***** | ****** | ****** | ***** | ****** | ***** | |
| *************************************** | | | | | | | |
| ANNU/ | AL TOTALS | FUK YEA | к 2008 | | | | |
| | | | | | | | |

| | ММ | CU. METERS | PERCENT |
|-------------------------------|------------|------------|---------|
| PRECIPITATION | 1190.50 | 11904.997 | 100.00 |
| RUNOFF | 289.549 | 2895.491 | 24.32 |
| EVAPOTRANSPIRATION | 759.741 | 7597.415 | 63.82 |
| PERC./LEAKAGE THROUGH LAYER 2 | 139.451508 | 1394.515 | 11.71 |
| AVG. HEAD ON TOP OF LAYER 2 | 31.2533 | | |
| PERC./LEAKAGE THROUGH LAYER 4 | 142.864883 | 1428.649 | 12.00 |
| CHANGE IN WATER STORAGE | -1.655 | -16.549 | -0.14 |
| SOIL WATER AT START OF YEAR | 1978.371 | 19783.711 | |
| SOIL WATER AT END OF YEAR | 1976.716 | 19767.162 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0008 | -0.008 | 0.00 |

AVERAGE MONTHLY VALUES (MM) FOR YEARS 1923 THROUGH 2022

| | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| PRECIPITATION | | | | | | |
| TOTALS | 108.32 70.25 | 125.65 70.88 | 140.77 62.27 | 121.45 75.55 | 100.17 86.71 | 120.21 91.16 |
| STD. DEVIATIONS | 74.48 65.33 | 85.28 74.25 | 94.50 50.54 | 101.89 56.69 | 75.37 62.89 | 96.67 65.51 |

| TOTALS | 20.291 | 33.925 | 44.198 | 46.268 | 36.351 | 55. |
|-----------------------|--------------|------------|----------|-----------|---------|-----|
| | 24.132 | 21.981 | 11.021 | 13.038 | | 12. |
| STD. DEVIATIONS | | 48.216 | | 76.800 | | 79. |
| | 46.841 | 54.676 | 27.433 | 28.988 | 34.583 | 30. |
| EVAPOTRANSPIRATION | | | | | | |
| TOTALS | | | 82.269 | | | 40. |
| | 36.777 | 39.093 | 42.627 | 60.263 | 67.524 | 71. |
| STD. DEVIATIONS | 32.632 | 32.902 | 31.660 | | | 11. |
| | 11.196 | 20.176 | 24.734 | 26.410 | 33.604 | 38. |
| PERCOLATION/LEAKAGE | THROUGH LAYE | R 2 | | | | |
| TOTALS | | | 12.9160 | | 19.1055 | |
| | 19.4139 | 12.5287 | 9.2291 | 8.9690 | 6.9101 | 6. |
| STD. DEVIATIONS | 6.2651 | | | | | |
| | 9.4630 | 10.4572 | 8.2783 | 6.8831 | 6.7659 | 6. |
| PERCOLATION/LEAKAGE | THROUGH LAYE | R 4 | | | | |
| TOTALS | 5.7761 | 8.2589 | | 15.3874 | 18.8044 | 20. |
| | 21.3463 | 14.8749 | 10.5675 | 9.1109 | 7.6024 | 6. |
| STD. DEVIATIONS | 5.6777 | | | | | |
| | 9.1327 | 10.1026 | 9.3094 | 6.9165 | 6.8030 | 6. |
| AVERAG | SES OF MONTH | ILY AVERAG | ED DAILY | HEADS (CM | 1) | |
| | | | | ` | · | |
| | | | | | | |
| DAILY AVERAGE HEAD ON | N TOP OF LAY | 'ER 2 | | | | |
| AVERAGES | | | 3.6390 | | 5.4014 | 6. |
| | 4.9623 | 3.1395 | 2.1090 | 1.9380 | 1.5595 | 1. |
| STD. DEVIATIONS | | | 3.1101 | | | |
| | | 2 2006 | 2 1721 | 2.1916 | 1 9//8 | 1 |

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1923 THROUGH 2022

| | MM | CU. METERS | PERCENT |
|--|-----------------------|------------|----------|
| PRECIPITATION | 1173.39 (283.704) | 11733.9 | 100.00 |
| RUNOFF | 332.568 (191.6273) | 3325.68 | 28.343 |
| EVAPOTRANSPIRATION | 689.908 (108.2144) | 6899.08 | 58.796 |
| PERCOLATION/LEAKAGE THROUGH LAYER 2 | 150.92529 (34.15227) | 1509.253 | 12.86238 |
| AVERAGE HEAD ON TOP OF LAYER 2 | 33.902 (10.376) | | |
| PERCOLATION/LEAKAGE THROUGH LAYER 4 | 150.92433 (34.71054) | 1509.243 | 12.86230 |
| CHANGE IN WATER STORAGE | -0.014 (0.8893) | -0.14 | -0.001 |

PEAK DAILY VALUES FOR YEARS 1923 THROUGH 2022

| | | (MM) | (CU. METERS) |
|-----------------------------------|---|----------|--------------|
| PRECIPITATION | | 150.40 | 1504.000 |
| RUNOFF | | 143.792 | 1437.9207 |
| PERCOLATION/LEAKAGE THROUGH LAYER | 2 | 1.007985 | 10.07985 |
| AVERAGE HEAD ON TOP OF LAYER 2 | | 150.000 | |
| PERCOLATION/LEAKAGE THROUGH LAYER | 4 | 1.512899 | 15.12899 |
| SNOW WATER | | 0.00 | 0.0000 |
| MAXIMUM VEG. SOIL WATER (VOL/VOL) | | 0.4 | 4630 |
| MINIMUM VEG. SOIL WATER (VOL/VOL) | | 0.: | 1160 |

| ^ |
|---|
| *************************************** |

FINAL WATER STORAGE AT END OF YEAR 2022

| LAYER | (CM) | (VOL/VOL) | |
|---|----------|-----------|--|
| 1 | 1.8741 | 0.1249 | |
| 2 | 38.4300 | 0.4270 | |
| 3 | 11.1292 | 0.3710 | |
| 4 | 145.9694 | 0.2919 | |
| SNOW WATER | 0.000 | | |
| *************************************** | | | |

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| ******** | *************************************** | ******* |
| ******** | *************************************** | ****** |
| ** | | ** |
| ** | | ** |
| ** | HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE | ** |
| ** | HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) | ** |
| ** | DEVELOPED BY ENVIRONMENTAL LABORATORY | ** |
| ** | USAE WATERWAYS EXPERIMENT STATION | ** |
| ** | FOR USEPA RISK REDUCTION ENGINEERING LABORATORY | ** |
| ** | | ** |
| ** | | ** |
| ******* | *************************************** | ******* |
| ******* | *************************************** | ******* |

| PRECIPITATION DATA FILE: | \WOY.D4 |
|----------------------------|--------------|
| TEMPERATURE DATA FILE: | \WOY.D7 |
| SOLAR RADIATION DATA FILE: | \WOY.D13 |
| EVAPOTRANSPIRATION DATA: | \WOY15.D11 |
| SOIL AND DESIGN DATA FILE: | \FIN1BAT.D10 |
| OUTPUT DATA FILE: | \FIN1BAT.OUT |

TIME: 17:34 DATE: 3/22/2023

TITLE: Final Cap Option 1 - BATTER

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 8 THICKNESS 15.00 CM = POROSITY 0.4630 VOL/VOL = FIELD CAPACITY 0.2320 VOL/VOL = WILTING POINT 0.1160 VOL/VOL = INITIAL SOIL WATER CONTENT = 0.1348 VOL/VOL EFFECTIVE SAT. HYD. COND. = 0.369999994000E-03 CM/SEC NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 1.80 FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2

TYPE 3 - BARRIER SOIL LINER
MATERIAL TEXTURE NUMBER 0THICKNESS=90.00 CMPOROSITY=0.4270 VOL/VOLFIELD CAPACITY=0.4180 VOL/VOLWILTING POINT=0.3670 VOL/VOLINITIAL SOIL WATER CONTENT=0.4270 VOL/VOLEFFECTIVE SAT. HYD. COND.=0.999999997000E-06 CM/SEC

LAYER 3

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 14

| THICKNESS | = | 30.00 CM |
|----------------------------|---|---------------------------|
| POROSITY | = | 0.4790 VOL/VOL |
| FIELD CAPACITY | = | 0.3710 VOL/VOL |
| WILTING POINT | = | 0.2510 VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.3710 VOL/VOL |
| EFFECTIVE SAT. HYD. COND. | = | 0.249999994000E-04 CM/SEC |

LAYER 4

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 18

| MATE | NIAL ILVIONE | NUMBER 10 | |
|--------------------|--------------|------------|-----------------|
| THICKNESS | = | 500.00 | CM |
| POROSITY | = | 0.6710 | VOL/VOL |
| FIELD CAPACITY | = | 0.2920 | VOL/VOL |
| WILTING POINT | = | 0.0770 | VOL/VOL |
| INITIAL SOIL WATER | CONTENT = | 0.2919 | VOL/VOL |
| EFFECTIVE SAT. HYD | . COND. = | 0.10000009 | 5000E-02 CM/SEC |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT SOIL DATA BASE USING SOIL TEXTURE # 8 WITH A POOR STAND OF GRASS, A SURFACE SLOPE OF 15.% AND A SLOPE LENGTH OF 90. METERS.

| SCS RUNOFF CURVE NUMBER | = | 86.50 | |
|------------------------------------|---|---------|----------|
| FRACTION OF AREA ALLOWING RUNOFF | = | 90.0 | PERCENT |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 1.0000 | HECTARES |
| EVAPORATIVE ZONE DEPTH | = | 15.0 | СМ |
| INITIAL WATER IN EVAPORATIVE ZONE | = | 2.022 | CM |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 6.945 | CM |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 1.740 | CM |
| INITIAL SNOW WATER | = | 0.000 | CM |
| INITIAL WATER IN LAYER MATERIALS | = | 197.544 | CM |
| TOTAL INITIAL WATER | = | 197.544 | CM |
| TOTAL SUBSURFACE INFLOW | = | 0.00 | MM/YR |

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM Woy Woy NSW

| STATION LATITUDE | = | -33.51 | DEGREES |
|---------------------------------------|---|--------|---------|
| MAXIMUM LEAF AREA INDEX | = | 1.00 | |
| START OF GROWING SEASON (JULIAN DATE) | = | 275 | |
| END OF GROWING SEASON (JULIAN DATE) | = | 91 | |
| EVAPORATIVE ZONE DEPTH | = | 15.0 | CM |
| AVERAGE ANNUAL WIND SPEED | = | 12.70 | KPH |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 66.70 | % |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 60.80 | % |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 72.30 | % |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 67.20 | % |

NOTE: PRECIPITATION DATA FOR

WAS ENTERED BY THE USER.

NOTE: TEMPERATURE DATA FOR

WAS ENTERED BY THE USER.

NOTE: SOLAR RADIATION DATA FOR

WAS ENTERED BY THE USER.

| *************************************** | | | | | | | |
|---|----------------|----------|----------------|---------|----------------|---------------|--|
| MONTHLY TOTALS (MM) FOR YEAR 1952 | | | | | | | |
| | | | | | | | |
| | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | | |
| JUN/DEC | | | | | | | |
| | | 20 0 | 220 0 | 220 7 | 15 C | 111 / | |
| PRECIPITATION | | | 228.0 24.4 | 115.1 | | 111.4 50.1 | |
| RUNOFF | 1.06 246.41 | 0.00 | 120.48 0.00 | | 0.00 0.00 | 48.51 0.00 | |
| | | | | | | | |
| EVAPOTRANSPIRATION | | | 82.72 22.13 | | | | |
| PERCOLATION/LEAKAGE THROUGH | 4.787 | 0.000 | 7.904 | 29.387 | 28.833 | | |
| LAYER 2 0.000 | 12.566 | 30.153 | 1.980 | 14.887 | 0.878 | | |
| PERCOLATION/LEAKAGE THROUGH | 8.049 | 0.000 | 0.000 | 24.156 | 29.791 | | |
| 16.288 LAYER 4 | | | 14.789 | 6.723 | 8.614 | | |
| 0.000 | | | | | | | |
| | | | | | | | |
| MONTHLY SU | JMMARIES H | FOR DAIL | Y HEADS | (CM) | | | |
| | | | | | | | |
| | | | | | | | |
| AVERAGE DAILY HEAD ON TOP OF LAYER 2 | | | | | 6.887 0.047 | | |
| STD. DEVIATION OF DAILY | 1.535 | 0.000 | 4.738 | 3.674 | 2.795 | 5.365 | |

HEAD ON TOP OF LAYER 2 5.226 3.609 0.473 4.272 0.260 0.000

ANNUAL TOTALS FOR YEAR 1952

| | MM | CU. METERS | PERCENT |
|-------------------------------|------------|------------|---------|
| PRECIPITATION | 1701.50 | 17014.996 | 100.00 |
| RUNOFF | 914.561 | 9145.612 | 53.75 |
| EVAPOTRANSPIRATION | 629.264 | 6292.644 | 36.98 |
| PERC./LEAKAGE THROUGH LAYER 2 | 147.952194 | 1479.522 | 8.70 |
| AVG. HEAD ON TOP OF LAYER 2 | 37.9559 | | |
| PERC./LEAKAGE THROUGH LAYER 4 | 151.097153 | 1510.972 | 8.88 |
| CHANGE IN WATER STORAGE | 6.578 | 65.775 | 0.39 |
| SOIL WATER AT START OF YEAR | 1975.755 | 19757.551 | |
| SOIL WATER AT END OF YEAR | 1982.333 | 19823.326 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0007 | -0.007 | 0.00 |
| | | | |

MONTHLY TOTALS (MM) FOR YEAR 2008
_____ JAN/JUL FEB/AUG MAR/SEP APR/OCT MAY/NOV JUN/DEC ----- ----- ----- ------ -----_ _ _ _ _ _ _ _ PRECIPITATION 106.7 257.2 46.3 166.1 13.5 164.3 55.0 47.0 99.9 69.6 76.1 88.8 25.53 102.47 0.00 58.81 0.00 RUNOFF 70.27 0.74 0.00 38.91 0.01 0.05 5.07 70.73 106.51 72.11 54.83 33.25 51.94 EVAPOTRANSPIRATION 30.23 46.78 64.05 69.76 54.52 94.45 10.440 18.531 3.786 20.593 8.639 PERCOLATION/LEAKAGE THROUGH 26.069 LAYER 2 12.558 11.878 14.040 2.123 0.560 8.516 PERCOLATION/LEAKAGE THROUGH 8.120 20.347 10.800 7.075 20.235 14.763 LAYER 4 17.848 15.617 12.859 6.795 0.610 5.975 MONTHLY SUMMARIES FOR DAILY HEADS (CM) _____ 2.946 6.822 0.387 7.005 1.424 AVERAGE DAILY HEAD ON 9.518 TOP OF LAYER 2 1.541 1.150 3.751 0.009 0.001 1.036 STD. DEVIATION OF DAILY 4.769 5.919 0.974 5.204 2.538 4.304 HEAD ON TOP OF LAYER 2 2.000 1.740 4.980 0.028 0.007 2.336 ANNUAL TOTALS FOR YEAR 2008 _____ CU. METERS PERCENT MM -----

| PRECIPITATION | 1190.50 | 11904.997 | 100.00 |
|-------------------------------|------------|-----------|--------|
| RUNOFF | 301.859 | 3018.588 | 25.36 |
| EVAPOTRANSPIRATION | 749.148 | 7491.476 | 62.93 |
| PERC./LEAKAGE THROUGH LAYER 2 | 137.731537 | 1377.315 | 11.57 |
| AVG. HEAD ON TOP OF LAYER 2 | 29.6577 | | |
| PERC./LEAKAGE THROUGH LAYER 4 | 141.043152 | 1410.432 | 11.85 |
| CHANGE IN WATER STORAGE | -1.550 | -15.495 | -0.13 |
| SOIL WATER AT START OF YEAR | 1978.367 | 19783.670 | |
| SOIL WATER AT END OF YEAR | 1976.818 | 19768.176 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0004 | -0.004 | 0.00 |
| | | | |

AVERAGE MONTHLY VALUES (MM) FOR YEARS 1923 THROUGH 2022

| | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------|---------|---------|---------|---------|---------|---------|
| PRECIPITATION | | | | | | |
| TOTALS | 108.32 | 125.65 | 140.77 | 121.45 | 100.17 | 120.21 |
| | 70.25 | 70.88 | 62.27 | 75.55 | 86.71 | 91.16 |
| STD. DEVIATIONS | 74.48 | 85.28 | 94.50 | 101.89 | 75.37 | 96.67 |
| | 65.33 | 74.25 | 50.54 | 56.69 | 62.89 | 65.51 |

RUNOFF

| TOTALS | 21.345 24.562 | 34.838 22.357 | 45.176 11.419 | 47.585 13.485 | 37.270 14.074 | 56.228 13.799 |
|--|--|---|--------------------------------------|--------------------------------------|--------------------------------------|-------------------------|
| STD. DEVIATIONS | 43.401 47.292 | 48.707 54.885 | 67.283 27.854 | 78.382 29.469 | 54.477 35.506 | 80.112 31.053 |
| EVAPOTRANSPIRATION | | | | | | |
| | 76 070 | 77 600 | 01 570 | 50 100 | 42 706 | 20.226 |
| TOTALS | 76.078 36.366 | 77.608 38.681 | 81.578 42.434 | 50.166 59.910 | 42.796 66.958 | 39.336 70.539 |
| STD. DEVIATIONS | 32.197 11.150 | 32.828 19.929 | 31.550 24.342 | 18.470 26.253 | 13.110 33.355 | 11.062 38.221 |
| PERCOLATION/LEAKAGE T | HROUGH LAYE | R 2 | | | | |
| TOTALS | 7 1460 | 0 7060 | 12 6400 | 17 5500 | 10 0471 | 20 720 |
| TUTALS | 19.1682 | 9.7060 12.3694 | 9.1277 | 8.8665 | 18.9471 6.7535 | 20.730 5.797 |
| STD. DEVIATIONS | 6.0404 9.4769 | | 8.6151 8.1928 | 9.9178 6.8479 | | 9.810 6.533 |
| PERCOLATION/LEAKAGE T | HROUGH LAYE | R 4 | | | | |
| TOTALS | 5.6599 | 8.0598 | 11.9425 | 15.1715 | 18.6141 | 20.029 |
| | 21.0506 | 14.7999 | 10.6083 | 8.9371 | 7.3913 | 6.545 |
| STD. DEVIATIONS | 5.4245 | 6.3244 | 8.5983 | 9.4021 | 9.2588 | 9.322 |
| | 9.2767 | 9.9192 | 9.2685 | 6.7751 | 6.6500 | 6.127 |
| | | | | | | |
| AVERAG | ES OF MONTH | LY AVERAG | ED DAILY | HEADS (CM |) | |
| AVERAG | ES OF MONTH | ILY AVERAG | ED DAILY | HEADS (CM |) | |
| | | | ED DAILY | HEADS (CM |) | |
| DAILY AVERAGE HEAD ON | TOP OF LAY | ′ER 2 | | | | 6.609 |
| | TOP OF LAY 1.6713 | | | 4.9429 | 5.2588 | |
| DAILY AVERAGE HEAD ON | TOP OF LAY 1.6713 4.8123 1.7747 | ÉR 2 2.8531 3.0294 2.7704 | 3.4576 2.0457 2.9837 | 4.9429 1.8680 3.8013 | 5.2588 1.4669 3.7332 | 6.609 1.166 4.063 |
| DAILY AVERAGE HEAD ON AVERAGES | TOP OF LAY 1.6713 4.8123 1.7747 | ÉR 2 2.8531 3.0294 2.7704 | 3.4576 2.0457 | 4.9429 1.8680 3.8013 | 5.2588 1.4669 | 1.166 |
| DAILY AVERAGE HEAD ON AVERAGES STD. DEVIATIONS | TOP OF LAY 1.6713 4.8123 1.7747 3.6252 | ZER 2 2.8531 3.0294 2.7704 3.2933 | 3.4576 2.0457 2.9837 2.4174 | 4.9429 1.8680 3.8013 2.1082 | 5.2588 1.4669 3.7332 1.8322 | 1.166 4.063 1.765 |
| DAILY AVERAGE HEAD ON AVERAGES | TOP OF LAY 1.6713 4.8123 1.7747 3.6252 | ZER 2 2.8531 3.0294 2.7704 3.2933 | 3.4576 2.0457 2.9837 2.4174 | 4.9429 1.8680 3.8013 2.1082 | 5.2588 1.4669 3.7332 1.8322 | 1.166 4.063 1.765 |
| DAILY AVERAGE HEAD ON AVERAGES STD. DEVIATIONS | TOP OF LAY 1.6713 4.8123 1.7747 3.6252 | ZER 2 2.8531 3.0294 2.7704 3.2933 | 3.4576 2.0457 2.9837 2.4174 | 4.9429 1.8680 3.8013 2.1082 | 5.2588 1.4669 3.7332 1.8322 | 1.166 4.063 1.765 |

| | | | . . |
|--|-----------------------|-------------------|--------------------|
| | MM | CU. METERS PERCEN | 4 I |
| PRECIPITATION | 1173.39 (283.704) | 11733.9 100.00 | |
| RUNOFF | 342.138 (193.1760) | 3421.38 29.158 | 3 |
| EVAPOTRANSPIRATION | 682.450 (107.1736) | 6824.50 58.161 | L |
| PERCOLATION/LEAKAGE THROUGH LAYER 2 | 148.81273 (33.77270) | 1488.127 12.682 | 234 |
| AVERAGE HEAD ON TOP OF LAYER 2 | 32.652 (10.118) | | |
| PERCOLATION/LEAKAGE THROUGH LAYER 4 | 148.80998 (34.26350) | 1488.100 12.682 | 210 |
| CHANGE IN WATER STORAGE | -0.013 (0.8493) | -0.13 -0.001 | L |
| ***** | ****** | ***** | ** |

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1923 THROUGH 2022

PEAK DAILY VALUES FOR YEARS 1923 THROUGH 2022 -----. (MM) (CU. METERS) -----_____ PRECIPITATION 1504.000 150.40 147.803 1478.0273 RUNOFF PERCOLATION/LEAKAGE THROUGH LAYER 2 1.007985 10.07985 AVERAGE HEAD ON TOP OF LAYER 2 150.000 PERCOLATION/LEAKAGE THROUGH LAYER 4 1.514090 15.14090 0.00 SNOW WATER 0.0000 MAXIMUM VEG. SOIL WATER (VOL/VOL) 0.4630 MINIMUM VEG. SOIL WATER (VOL/VOL) 0.1160

♠ ******* FINAL WATER STORAGE AT END OF YEAR 2022 _____ (VOL/VOL) (CM) LAYER ----1 1.8690 0.1246 2 38.4300 0.4270 3 11.1296 0.3710 4 145.9896 0.2920 SNOW WATER 0.000

| ♠ | | |
|-----------|---|---------|
| ********* | *************************************** | ******* |
| ********* | *************************************** | ******* |
| ** | | ** |
| ** | | ** |
| ** | HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE | ** |
| ** | HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) | ** |
| ** | DEVELOPED BY ENVIRONMENTAL LABORATORY | ** |
| ** | USAE WATERWAYS EXPERIMENT STATION | ** |
| ** | FOR USEPA RISK REDUCTION ENGINEERING LABORATORY | ** |
| ** | | ** |
| ** | | ** |
| ********* | *************************************** | ******* |
| ********* | *************************************** | ******* |

| PRECIPITATION DATA FILE: | \WOY.D4 |
|----------------------------|---------------|
| TEMPERATURE DATA FILE: | \WOY.D7 |
| SOLAR RADIATION DATA FILE: | \WOY.D13 |
| EVAPOTRANSPIRATION DATA: | \WOY30.D11 |
| SOIL AND DESIGN DATA FILE: | \FIN2BPLT.D10 |
| OUTPUT DATA FILE: | \FIN2BPLT.OUT |

TIME: 17:55 DATE: 3/22/2023

TITLE: Final Cap Option 2B - PLATFORM

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 8 THICKNESS 20.00 CM = POROSITY 0.4630 VOL/VOL = FIELD CAPACITY 0.2320 VOL/VOL = WILTING POINT 0.1160 VOL/VOL = 0.1479 VOL/VOL INITIAL SOIL WATER CONTENT =

EFFECTIVE SAT. HYD. COND. = 0.369999994000E-03 CM/SEC NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00 FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2

TYPE 2 - LATERAL DRAINAGE LAYER

| MATERIAL TEX | TURE | NUMBER 10 | |
|----------------------------|------|-------------|-----------------|
| THICKNESS | = | 80.00 | CM |
| POROSITY | = | 0.3980 | VOL/VOL |
| FIELD CAPACITY | = | 0.2440 | VOL/VOL |
| WILTING POINT | = | 0.1360 | VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.3626 | VOL/VOL |
| EFFECTIVE SAT. HYD. COND. | = | 0.119999993 | 7000E-03 CM/SEC |
| SLOPE | = | 5.00 | PERCENT |
| DRAINAGE LENGTH | = | 225.0 | METERS |
| | | | |

LAYER 3

TYPE 4 - FLEXIBLE MEMBRANE LINER MATERIAL TEXTURE NUMBER 36

| THICKNESS | = | 0.20 CM |
|----------------------------|---|---------------------------|
| POROSITY | = | 0.0000 VOL/VOL |
| FIELD CAPACITY | = | 0.0000 VOL/VOL |
| WILTING POINT | = | 0.0000 VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0000 VOL/VOL |
| EFFECTIVE SAT. HYD. COND. | = | 0.399999993000E-12 CM/SEC |
| FML PINHOLE DENSITY | = | 0.00 HOLES/HECTARE |
| FML INSTALLATION DEFECTS | = | 0.00 HOLES/HECTARE |
| FML PLACEMENT QUALITY | = | 4 - POOR |
| | | |

LAYER 4

| | TYPE 3 - BA | | | | |
|----------------|--------------|-------|------------|----------|--------|
| | MATERIAL TE | XTURE | NUMBER 17 | | |
| THICKNESS | | = | 0.60 | СМ | |
| POROSITY | | = | 0.7500 | VOL/VOL | |
| FIELD CAPACIT | Y | = | 0.7470 | VOL/VOL | |
| WILTING POINT | | = | 0.4000 | VOL/VOL | |
| INITIAL SOIL N | WATER CONTEN | T = | 0.7500 | VOL/VOL | |
| EFFECTIVE SAT | . HYD. COND. | = | 0.30000003 | 3000E-08 | CM/SEC |

LAYER 5

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 14 THICKNESS = 30.00 CM POROSITY 0.4790 VOL/VOL = = FIELD CAPACITY 0.3710 VOL/VOL WILTING POINT 0.2510 VOL/VOL = INITIAL SOIL WATER CONTENT = 0.3710 VOL/VOL EFFECTIVE SAT. HYD. COND. = 0.249999994000E-04 CM/SEC

LAYER 6

TYPE 1 - VERTICAL PERCOLATION LAYER

| MATERIAL | TEXTURE | NUMBER | 18 |
|----------|---------|--------|----|
|----------|---------|--------|----|

| THI | CKNESS | = | 500.00 CM |
|-----|-------------------------|---|---------------------------|
| POR | OSITY | = | 0.6710 VOL/VOL |
| FIE | LD CAPACITY | = | 0.2920 VOL/VOL |
| WIL | TING POINT | = | 0.0770 VOL/VOL |
| INI | TIAL SOIL WATER CONTENT | = | 0.2919 VOL/VOL |
| EFF | ECTIVE SAT. HYD. COND. | = | 0.100000005000E-02 CM/SEC |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT SOIL DATA BASE USING SOIL TEXTURE # 8 WITH A FAIR STAND OF GRASS, A SURFACE SLOPE OF 5.% AND A SLOPE LENGTH OF 225. METERS.

| SCS RUNOFF CURVE NUMBER | = | 78.70 | |
|------------------------------------|---|---------|----------|
| FRACTION OF AREA ALLOWING RUNOFF | = | 75.0 | PERCENT |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 1.0000 | HECTARES |
| EVAPORATIVE ZONE DEPTH | = | 30.0 | СМ |
| INITIAL WATER IN EVAPORATIVE ZONE | = | 4.322 | СМ |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 13.240 | CM |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 3.680 | СМ |
| INITIAL SNOW WATER | = | 0.000 | СМ |
| INITIAL WATER IN LAYER MATERIALS | = | 189.492 | CM |
| TOTAL INITIAL WATER | = | 189.492 | СМ |
| TOTAL SUBSURFACE INFLOW | = | 0.00 | MM/YR |

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM Woy Woy NSW

| STATION LATITUDE | = | -33.51 | DEGREES |
|---------------------------------------|---|--------|---------|
| MAXIMUM LEAF AREA INDEX | = | 2.00 | |
| START OF GROWING SEASON (JULIAN DATE) | = | 275 | |
| END OF GROWING SEASON (JULIAN DATE) | = | 91 | |
| EVAPORATIVE ZONE DEPTH | = | 30.0 | CM |
| AVERAGE ANNUAL WIND SPEED | = | 12.70 | КРН |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 66.70 | % |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 60.80 | % |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 72.30 | % |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 67.20 | % |

NOTE: PRECIPITATION DATA FOR

WAS ENTERED BY THE USER.

NOTE: TEMPERATURE DATA FOR

WAS ENTERED BY THE USER.

NOTE: SOLAR RADIATION DATA FOR

WAS ENTERED BY THE USER.

MONTHLY TOTALS (MM) FOR YEAR 1952

| | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | |
|---|------------------|------------------|---------------|----------------|----------------|------------------|
| JUN/DEC | | | | | | |
| | | | | | | |
| PRECIPITATION | 46.4 317.4 | 28.0 371.3 | 228.0 24.4 | 320.7 115.1 | 45.6 43.1 | 111.4 50.1 |
| RUNOFF | 0.00 | 0.00 | 73.00 | 222.01 | 9.28 | 65.08 |
| | 257.37 | 322.14 | 0.00 | 3.50 | 0.00 | 0.00 |
| EVAPOTRANSPIRATION | | | | | 48.16 93.84 | |
| LATERAL DRAINAGE COLLECTED | 0.976 | 0.905 | 1.398 | 2.979 | 2.816 | |
| 2.485 FROM LAYER 2 0.986 | 2.269 | 3.036 | 1.479 | 1.900 | 1.015 | |
| PERCOLATION/LEAKAGE THROUGH | 0.004 | 0.003 | 0.004 | 0.005 | 0.005 | |
| 0.005 LAYER 4 0.004 | 0.005 | 0.005 | 0.004 | 0.005 | 0.004 | |
| PERCOLATION/LEAKAGE THROUGH 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| LAYER 6 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | | | | | | |
| | | | | | | |
| MONTHLY SU | IMMARIES | FOR DAIL | Y HEADS | (CM) | | |
| | | | | | | |
| AVERAGE DAILY HEAD ON TOP OF LAYER 3 | 68.478 91.907 | 67.867 97.731 | | | | 94.174 69.232 |
| STD. DEVIATION OF DAILY | | 0.168 | | | | |
| HEAD ON TOP OF LAYER 3 | 4.179 | 2.478 | 2.053 | 5.125 | 4.998 | 0.187 |
| *************************************** | | | | | | |
| | | | | | | |
| | | | | | | |
| *************************************** | | | | | | |
| ANNUA | L TOTALS | FOR YEAI | R 1952 | | | |
| | | | | | | |

| | ММ | CU. METERS | PERCENT |
|---------------------------------|----------|------------|---------|
| PRECIPITATION | 1701.50 | 17014.996 | 100.00 |
| RUNOFF | 952.365 | 9523.651 | 55.97 |
| EVAPOTRANSPIRATION | 716.953 | 7169.527 | 42.14 |
| DRAINAGE COLLECTED FROM LAYER 2 | 22.2423 | 222.423 | 1.31 |
| PERC./LEAKAGE THROUGH LAYER 4 | 0.053003 | 0.530 | 0.00 |
| AVG. HEAD ON TOP OF LAYER 3 | 837.6210 | | |
| PERC./LEAKAGE THROUGH LAYER 6 | 0.00000 | 0.000 | 0.00 |
| CHANGE IN WATER STORAGE | 9.940 | 99.399 | 0.58 |
| SOIL WATER AT START OF YEAR | 1889.080 | 18890.801 | |
| SOIL WATER AT END OF YEAR | 1899.020 | 18990.199 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0004 | -0.004 | 0.00 |

MONTHLY TOTALS (MM) FOR YEAR 2008

 JAN/JUL
 FEB/AUG
 MAR/SEP
 APR/OCT
 MAY/NOV

 JUN/DEC
 ----- ----- ----- -----

 PRECIPITATION
 106.7
 257.2
 46.3
 166.1
 13.5
 164.3

| | 55.0 | 47.0 | 99.9 | 69.6 | 76.1 | 88.8 |
|--------------------------------------|----------------|-----------------|-----------------|-----------------|----------------|-----------------|
| RUNOFF | 0.00 14.21 | 77.72 0.00 | 0.00 67.08 | 38.73 0.00 | 0.00 0.00 | 120.13 0.29 |
| EVAPOTRANSPIRATION | 93.25 32.56 | 131.94 48.53 | 114.18 65.69 | 34.38 105.17 | 20.70 71.16 | 33.97 107.77 |
| LATERAL DRAINAGE COLLECTED 3.102 | 1.185 | 2.152 | 1.110 | 1.681 | 2.715 | |
| FROM LAYER 2 1.004 | 2.717 | 2.609 | 2.323 | 1.357 | 0.967 | |
| PERCOLATION/LEAKAGE THROUGH 0.005 | 0.004 | 0.005 | 0.004 | 0.004 | 0.005 | |
| LAYER 4 0.004 | 0.005 | 0.005 | 0.005 | 0.004 | 0.004 | |
| PERCOLATION/LEAKAGE THROUGH 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| LAYER 6 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |

MONTHLY SUMMARIES FOR DAILY HEADS (CM)

| AVERAGE DAILY HEAD ON TOP OF LAYER 3 | 91.037 94.490 | | |
|---|--------------------|------|------|
| STD. DEVIATION OF DAILY HEAD ON TOP OF LAYER 3 | 8.261 2.379 | | |

ANNUAL TOTALS FOR YEAR 2008

| | MM | CU. METERS | PERCENT |
|---------------|---------|------------|---------|
| | | | |
| PRECIPITATION | 1190.50 | 11904.997 | 100.00 |
| RUNOFF | 318.155 | 3181.549 | 26.72 |

| EVAPOTRANSPIRATION | 859.298 | 8592.978 | 72.18 |
|---------------------------------|----------|-----------|-------|
| DRAINAGE COLLECTED FROM LAYER 2 | 22.9212 | 229.212 | 1.93 |
| PERC./LEAKAGE THROUGH LAYER 4 | 0.053968 | 0.540 | 0.00 |
| AVG. HEAD ON TOP OF LAYER 3 | 853.6609 | | |
| PERC./LEAKAGE THROUGH LAYER 6 | 0.00000 | 0.000 | 0.00 |
| CHANGE IN WATER STORAGE | -9.874 | -98.736 | -0.83 |
| SOIL WATER AT START OF YEAR | 1901.890 | 19018.896 | |
| SOIL WATER AT END OF YEAR | 1892.016 | 18920.160 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0005 | -0.005 | 0.00 |
| | | | |

AVERAGE MONTHLY VALUES (MM) FOR YEARS 1923 THROUGH 2022

| | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| PRECIPITATION | | | | | | |
| TOTALS | 108.32 70.25 | 125.65 70.88 | 140.77 62.27 | 121.45 75.55 | 100.17 86.71 | 120.21 91.16 |
| STD. DEVIATIONS | 74.48 65.33 | 85.28 74.25 | 94.50 50.54 | 101.89 56.69 | 75.37 62.89 | 96.67 65.51 |
| RUNOFF | | | | | | |
| TOTALS | 10.784 | 21.206 | 34.933 | 47.617 | 47.149 | 76.116 |

| | 36.921 | 30.502 | 14.902 | 14.092 | 8.038 | 6.461 |
|-----------------------|--------------|------------------|------------------|------------------|------------------|------------------|
| STD. DEVIATIONS | 33.232 | 39.984 61.805 | 64.318 33.163 | 83.238 30.209 | 59.790 28.252 | 88.958 20.694 |
| | 55.0/1 | 01.005 | 22.102 | 50.209 | 20,252 | 20.094 |
| EVAPOTRANSPIRATION | | | | | | |
| TOTALS | | 91.770 | | 45.718 | | 35.530 |
| | 37.294 | 48.387 | 50.495 | 96.811 | 88.220 | 84.309 |
| STD. DEVIATIONS | 41.512 | 37.461 | | | 9.221 | |
| | 5.124 | 12.458 | 22.404 | 19.699 | 43.202 | 45.983 |
| ATERAL DRAINAGE COLL | ECTED FROM | LAYER 2 | | | | |
| TOTALS | 1.1573 | 1.2427 | 1.5465 | 1.9153 | 2.4455 | 2.6680 |
| | 2.6586 | 2.2294 | 1.7757 | 1.5903 | 1.1707 | 1.1372 |
| STD. DEVIATIONS | 0.2993 | 0.4517 | 0.5783 | 0.7891 | 0.7116 | 0.5464 |
| | 0.4478 | | | | | |
| PERCOLATION/LEAKAGE 1 | HROUGH LAYE | R 4 | | | | |
| TOTALS | 0.0039 | 0.0037 | 0.0043 | 0.0044 | 0.0049 | 0.0049 |
| | 0.0051 | | 0.0046 | 0.0045 | 0.0039 | 0.0039 |
| STD. DEVIATIONS | 0.0003 | 0.0004 | 0.0005 | 0.0006 | 0.0005 | 0.0003 |
| | 0.0002 | 0.0003 | | 0.0002 | 0.0003 | 0.0003 |
| PERCOLATION/LEAKAGE 1 | HROUGH LAYE | R 6 | | | | |
| TOTALS | 0.0000 | 0.0000 | 0.0000 | 0.0122 | 0.0060 | 0.0062 |
| | 0.0000 | | 0.0000 | 0.0122 | 0.0122 | 0.0000 |
| STD. DEVIATIONS | 0.0000 | 0.0000 | 0.0000 | 0.0856 | 0.0600 | 0.0608 |
| 5151 5212/12015 | 0.0000 | | | | | 0.0000 |
| | | | | | | |
| AVERAG | ES OF MONTH | ILY AVERAG | ED DAILY | HEADS (CM | I) | |
| | | | | · | | |
| | | | | | | |
| DAILY AVERAGE HEAD ON | I TOP OF LAY | YER 3 | | | | |
| AVERAGES | 72.9832 | 76.5038 | 79.6441 | 85.1422 | 91.4712 | 95.0115 |
| | 94.5953 | 91.3784 | 88.2080 | 84.4645 | 74.4921 | 72.8184 |
| STD. DEVIATIONS | 5.5559 | 8.1215 | 8.7293 | 10.9462 | 8.4248 | 6.1281 |
| | | 4.7054 | | | 6.4924 | |

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1923 THROUGH 2022

| | Mi | М | CU. METERS | PERCENT | | |
|--|-------------|----------------|------------|---------|--|--|
| PRECIPITATION | 1173.39 | (283.704) | 11733.9 | 100.00 | | |
| RUNOFF | 348.723 | (221.4369) | 3487.23 | 29.719 | | |
| EVAPOTRANSPIRATION | 803.120 | (117.0217) | 8031.20 | 68.445 | | |
| LATERAL DRAINAGE COLLECTED FROM LAYER 2 | 21.53731 | (2.68768) | 215.373 | 1.83548 | | |
| PERCOLATION/LEAKAGE THROUGH LAYER 4 | 0.05297 | (0.00194) | 0.530 | 0.00451 | | |
| AVERAGE HEAD ON TOP OF LAYER 3 | 838.927 (| 30.844) | | | | |
| PERCOLATION/LEAKAGE THROUGH LAYER 6 | 0.04866 | (0.16584) | 0.487 | 0.00415 | | |
| CHANGE IN WATER STORAGE | -0.043 | (1.3499) | -0.43 | -0.004 | | |
| ***** | ****** | ***** | ****** | ***** | | |
| ∧ ************************************ | | | | | | |
| PEAK DAILY VA | LUES FOR YE | ARS 1923 THROU | GH 2022 | | | |
| | | (MM) | (CU. ME | TERS) | | |
| PRECIPITATION | | 150.40 | 1504. | .000 | | |
| | | | | | | |

RUNOFF143.4121434.1163DRAINAGE COLLECTED FROM LAYER 20.107551.07555PERCOLATION/LEAKAGE THROUGH LAYER 40.0001730.00173AVERAGE HEAD ON TOP OF LAYER 3999.995

| MAXIMUM HEAD ON TOP OF LAYER 3 | 1551.996 | | | | |
|---|----------------------------|---------|--|--|--|
| LOCATION OF MAXIMUM HEAD IN LAYER (DISTANCE FROM DRAIN) | 2 50.0 METERS | | | | |
| PERCOLATION/LEAKAGE THROUGH LAYER | 6 0.608241 | 6.08241 | | | |
| SNOW WATER | 0.00 | 0.0000 | | | |
| MAXIMUM VEG. SOIL WATER (VOL/VOL) MINIMUM VEG. SOIL WATER (VOL/VOL) | 0.4413 0.1227 | | | | |
| *** Maximum heads are computed u | using McEnroe's equations. | *** | | | |
| Reference: Maximum Saturated Depth over Landfill Liner by Bruce M. McEnroe, University of Kansas ASCE Journal of Environmental Engineering Vol. 119, No. 2, March 1993, pp. 262-270. | | | | | |

FINAL WATER STORAGE AT END OF YEAR 2022

| LAYE | R (CM) | (VOL/VOL) | |
|--------|------------|-----------|--|
| 1 | 2.4461 | 0.1223 | |
| 2 | 29.0519 | 0.3631 | |
| 3 | 0.000 | 0.0000 | |
| 4 | 0.4500 | 0.7500 | |
| 5 | 11.1297 | 0.3710 | |
| 6 | 145.9863 | 0.2920 | |
| SNOW W | ATER 0.000 | | |

| ♠ | | |
|-----------|---|---------|
| ********* | *************************************** | ******* |
| ********* | *************************************** | ******* |
| ** | | ** |
| ** | | ** |
| ** | HYDROLOGIC EVALUATION OF LANDFILL PERFORMANCE | ** |
| ** | HELP MODEL VERSION 3.07 (1 NOVEMBER 1997) | ** |
| ** | DEVELOPED BY ENVIRONMENTAL LABORATORY | ** |
| ** | USAE WATERWAYS EXPERIMENT STATION | ** |
| ** | FOR USEPA RISK REDUCTION ENGINEERING LABORATORY | ** |
| ** | | ** |
| ** | | ** |
| ********* | *************************************** | ******* |
| ********* | *************************************** | ******* |

| PRECIPITATION DATA FILE: | \WOY.D4 |
|----------------------------|---------------|
| TEMPERATURE DATA FILE: | \WOY.D7 |
| SOLAR RADIATION DATA FILE: | \WOY.D13 |
| EVAPOTRANSPIRATION DATA: | \WOY30.D11 |
| SOIL AND DESIGN DATA FILE: | \FIN2BBAT.D10 |
| OUTPUT DATA FILE: | \FIN2BBAT.OUT |

TIME: 18: 1 DATE: 3/22/2023

TITLE: Final Cap Option 2B - BATTER

NOTE: INITIAL MOISTURE CONTENT OF THE LAYERS AND SNOW WATER WERE COMPUTED AS NEARLY STEADY-STATE VALUES BY THE PROGRAM.

LAYER 1

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 8 THICKNESS 20.00 CM = POROSITY 0.4630 VOL/VOL = FIELD CAPACITY 0.2320 VOL/VOL = WILTING POINT 0.1160 VOL/VOL = INITIAL SOIL WATER CONTENT = 0.1510 VOL/VOL EFFECTIVE SAT. HYD. COND. = 0.369999994000E-03 CM/SEC NOTE: SATURATED HYDRAULIC CONDUCTIVITY IS MULTIPLIED BY 3.00 FOR ROOT CHANNELS IN TOP HALF OF EVAPORATIVE ZONE.

LAYER 2

TYPE 2 - LATERAL DRAINAGE LAYER

| MATERIAL IE | XIURE | NOWBER 10 | |
|---------------------------|-------|-------------|-----------------|
| THICKNESS | = | 80.00 | CM |
| POROSITY | = | 0.3980 | VOL/VOL |
| FIELD CAPACITY | = | 0.2440 | VOL/VOL |
| WILTING POINT | = | 0.1360 | VOL/VOL |
| INITIAL SOIL WATER CONTEN | T = | 0.3458 | VOL/VOL |
| EFFECTIVE SAT. HYD. COND. | = | 0.119999997 | 7000E-03 CM/SEC |
| SLOPE | = | 15.00 | PERCENT |
| DRAINAGE LENGTH | = | 90.0 | METERS |
| | | | |

LAYER 3

TYPE 4 - FLEXIBLE MEMBRANE LINER MATERIAL TEXTURE NUMBER 36

| | ONE | NONDER 50 |
|----------------------------|-----|---------------------------|
| THICKNESS | = | 0.20 CM |
| POROSITY | = | 0.0000 VOL/VOL |
| FIELD CAPACITY | = | 0.0000 VOL/VOL |
| WILTING POINT | = | 0.0000 VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.0000 VOL/VOL |
| EFFECTIVE SAT. HYD. COND. | = | 0.399999993000E-12 CM/SEC |
| FML PINHOLE DENSITY | = | 0.00 HOLES/HECTARE |
| FML INSTALLATION DEFECTS | = | 0.00 HOLES/HECTARE |
| FML PLACEMENT QUALITY | = | 4 - POOR |
| | | |

LAYER 4

TYPE 3 - BARRIER SOIL LINER MATERIAL TEXTURE NUMBER 17

| THICKNESS | = | 0.60 CM |
|----------------------------|---|--------------------------|
| POROSITY | = | 0.7500 VOL/VOL |
| FIELD CAPACITY | = | 0.7470 VOL/VOL |
| WILTING POINT | = | 0.4000 VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.7500 VOL/VOL |
| EFFECTIVE SAT. HYD. COND. | = | 0.30000003000E-08 CM/SEC |

LAYER 5

TYPE 1 - VERTICAL PERCOLATION LAYER MATERIAL TEXTURE NUMBER 14 THICKNESS = 30.00 CM POROSITY 0.4790 VOL/VOL = = FIELD CAPACITY 0.3710 VOL/VOL WILTING POINT 0.2510 VOL/VOL = INITIAL SOIL WATER CONTENT = 0.3710 VOL/VOL EFFECTIVE SAT. HYD. COND. = 0.249999994000E-04 CM/SEC

LAYER 6

TYPE 1 - VERTICAL PERCOLATION LAYER

| MATERIAL | TEXTURE | NUMBER | 18 |
|----------|---------|--------|----|
|----------|---------|--------|----|

| THICKNESS | = | 500.00 CM |
|----------------------------|---|---------------------------|
| POROSITY | = | 0.6710 VOL/VOL |
| FIELD CAPACITY | = | 0.2920 VOL/VOL |
| WILTING POINT | = | 0.0770 VOL/VOL |
| INITIAL SOIL WATER CONTENT | = | 0.2919 VOL/VOL |
| EFFECTIVE SAT. HYD. COND. | = | 0.100000005000E-02 CM/SEC |

GENERAL DESIGN AND EVAPORATIVE ZONE DATA

NOTE: SCS RUNOFF CURVE NUMBER WAS COMPUTED FROM DEFAULT SOIL DATA BASE USING SOIL TEXTURE # 8 WITH A FAIR STAND OF GRASS, A SURFACE SLOPE OF 15.% AND A SLOPE LENGTH OF 90. METERS.

| SCS RUNOFF CURVE NUMBER | = | 80.30 | |
|------------------------------------|---|---------|----------|
| FRACTION OF AREA ALLOWING RUNOFF | = | 90.0 | PERCENT |
| AREA PROJECTED ON HORIZONTAL PLANE | = | 1.0000 | HECTARES |
| EVAPORATIVE ZONE DEPTH | = | 30.0 | CM |
| INITIAL WATER IN EVAPORATIVE ZONE | = | 4.384 | CM |
| UPPER LIMIT OF EVAPORATIVE STORAGE | = | 13.240 | CM |
| LOWER LIMIT OF EVAPORATIVE STORAGE | = | 3.680 | CM |
| INITIAL SNOW WATER | = | 0.000 | CM |
| INITIAL WATER IN LAYER MATERIALS | = | 188.210 | CM |
| TOTAL INITIAL WATER | = | 188.210 | CM |
| TOTAL SUBSURFACE INFLOW | = | 0.00 | MM/YR |

EVAPOTRANSPIRATION AND WEATHER DATA

NOTE: EVAPOTRANSPIRATION DATA WAS OBTAINED FROM Woy Woy NSW

| STATION LATITUDE | = | -33.51 | DEGREES |
|---------------------------------------|---|--------|---------|
| MAXIMUM LEAF AREA INDEX | = | 2.00 | |
| START OF GROWING SEASON (JULIAN DATE) | = | 275 | |
| END OF GROWING SEASON (JULIAN DATE) | = | 91 | |
| EVAPORATIVE ZONE DEPTH | = | 30.0 | CM |
| AVERAGE ANNUAL WIND SPEED | = | 12.70 | КРН |
| AVERAGE 1ST QUARTER RELATIVE HUMIDITY | = | 66.70 | % |
| AVERAGE 2ND QUARTER RELATIVE HUMIDITY | = | 60.80 | % |
| AVERAGE 3RD QUARTER RELATIVE HUMIDITY | = | 72.30 | % |
| AVERAGE 4TH QUARTER RELATIVE HUMIDITY | = | 67.20 | % |

NOTE: PRECIPITATION DATA FOR

WAS ENTERED BY THE USER.

NOTE: TEMPERATURE DATA FOR

WAS ENTERED BY THE USER.

NOTE: SOLAR RADIATION DATA FOR

WAS ENTERED BY THE USER.

MONTHLY TOTALS (MM) FOR YEAR 1952

JAN/JUL FEB/AUG MAR/SEP APR/OCT MAY/NOV

JUN/DEC

----- -----46.428.0228.0320.745.6111.4317.4371.324.4115.143.150.1 PRECIPITATION 0 00 0 00 EQ 27 10E 90 0 10 E1 20

| RUNOFF | 0.00 243.57 | 0.00 310.41 | 58.37 0.00 | 195.80 0.92 | 0.18 0.00 | 51.28 0.00 |
|--------------------------------------|----------------|----------------|----------------|-----------------|----------------|----------------|
| EVAPOTRANSPIRATION | 46.40 41.35 | 27.69 66.55 | 81.54 35.75 | 67.26 114.77 | 48.65 71.08 | 43.04 42.30 |
| LATERAL DRAINAGE COLLECTED | 6.140 | 5.377 | 7.957 | 21.001 | 18.852 | |
| FROM LAYER 2 6.706 | 13.771 | 21.298 | 9.109 | 10.099 | 7.011 | |
| PERCOLATION/LEAKAGE THROUGH 0.005 | 0.003 | 0.003 | 0.003 | 0.005 | 0.005 | |
| LAYER 4 0.003 | 0.005 | 0.005 | 0.004 | 0.004 | 0.004 | |
| PERCOLATION/LEAKAGE THROUGH 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| LAYER 6 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |

MONTHLY SUMMARIES FOR DAILY HEADS (CM)

| AVERAGE DAILY HEAD ON | 58,600 | 54.862 | 60.658 | 97.089 | 94.147 | 91.287 |
|-------------------------|---------------|--------|--------|--------|--------|--------|
| | | | | | | |
| TOP OF LAYER 3 | 88.639 | 96.674 | 82.394 | 81.666 | 69.148 | 64.002 |
| | | | | | | |
| | | | | | | |
| STD. DEVIATION OF DAILY | 1.171 | 1 025 | 17 286 | 4.156 | 2 822 | 4.858 |
| SID. DEVIATION OF DATE | T •T/T | 1.025 | 17.200 | 4.100 | 2.022 | +.0J0 |
| HEAD ON TOP OF LAYER 3 | 5.445 | 3,324 | 2,780 | 5.659 | 2.837 | 1.278 |
| | 5.115 | 2.221 | 2.700 | 5.055 | 2.05/ | 1.2/0 |

ANNUAL TOTALS FOR YEAR 1952

| ММ | CU. METERS | PERCENT |
|----|------------|---------|
| | | |

| PRECIPITATION | 1701.50 | 17014.996 | 100.00 |
|---------------------------------|----------|-----------|--------|
| RUNOFF | 860.523 | 8605.234 | 50.57 |
| EVAPOTRANSPIRATION | 686.378 | 6863.777 | 40.34 |
| DRAINAGE COLLECTED FROM LAYER 2 | 142.9020 | 1429.020 | 8.40 |
| PERC./LEAKAGE THROUGH LAYER 4 | 0.049533 | 0.495 | 0.00 |
| AVG. HEAD ON TOP OF LAYER 3 | 782.6395 | | |
| PERC./LEAKAGE THROUGH LAYER 6 | 0.00000 | 0.000 | 0.00 |
| CHANGE IN WATER STORAGE | 11.697 | 116.970 | 0.69 |
| SOIL WATER AT START OF YEAR | 1876.352 | 18763.518 | |
| SOIL WATER AT END OF YEAR | 1888.049 | 18880.486 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0005 | -0.005 | 0.00 |

 MONTHLY TOTALS (MM) FOR YEAR 2008

 JAN/JUL FEB/AUG MAR/SEP APR/OCT MAY/NOV

 JUN/DEC

 PRECIPITATION

 106.7
 257.2
 46.3
 166.1
 13.5
 164.3

 S5.0
 47.0
 99.9
 69.6
 76.1
 88.8

 RUNOFF
 0.03
 67.09
 0.00
 29.34
 0.00
 94.64

| EVAPOTRANSPIRATION | 86.39 32.23 | | 102.42 62.57 | 33.62 103.14 | | 30.59 100.91 |
|---|------------------|----------|------------------|-------------------|-----------|------------------|
| LATERAL DRAINAGE COLLECTED | 8.165 | 14.574 | 7.635 | 11.693 | 15.678 | |
| 21.247 FROM LAYER 2 6.906 | 15.836 | 14.838 | 14.192 | 8.535 | 6.859 | |
| • | 0.004 | 0.004 | 0.004 | 0.004 | 0.005 | |
| 0.005 LAYER 4 0.004 | 0.005 | 0.005 | 0.005 | 0.004 | 0.004 | |
| - | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| 0.000 LAYER 6 0.000 | 0.000 | 0.000 | 0.000 | 0.608 | 0.000 | |
| | | | | | | |
| MONTHLY SU | MMARTES | FOR DATL | Y HFADS | (CM) | | |
| | | | | | | |
| | | | | | | |
| AVERAGE DAILY HEAD ON TOP OF LAYER 3 | 73.856 91.032 | | 72.510 89.701 | 77.759 79.494 | | 97.353 65.917 |
| STD. DEVIATION OF DAILY HEAD ON TOP OF LAYER 3 | | | | 14.396 3.322 | | |
| ***** | ****** | ****** | ****** | * * * * * * * * * | ***** | ***** |
| | | | | | | |
| | | | | | | |
| *************************************** | | | | ****** | ****** | ***** |
| ANNUA | L TOTALS | FOR YEA | R 2008 | | | |
| | | MM | | CU. METI | ERS P | ERCENT |
| PRECIPITATION | | 1190.50 | | 11904.9 | 997 1 | 00.00 |
| RUNOFF | | 240.16 | 1 | 2401.0 | 515 | 20.17 |
| EVAPOTRANSPIRATION | | 812.74 | 1 | 8127.4 | 409 | 68.27 |
| DRAINAGE COLLECTED FROM LAYER | 2 | 146.15 | 98 | 1461.5 | 598 | 12.28 |

| PERC./LEAKAGE THROUGH LAYER 4 | 0.051893 | 0.519 | 0.00 |
|-------------------------------|----------|-----------|-------|
| AVG. HEAD ON TOP OF LAYER 3 | 820.9964 | | |
| PERC./LEAKAGE THROUGH LAYER 6 | 0.608223 | 6.082 | 0.05 |
| CHANGE IN WATER STORAGE | -9.170 | -91.702 | -0.77 |
| SOIL WATER AT START OF YEAR | 1895.263 | 18952.625 | |
| SOIL WATER AT END OF YEAR | 1886.092 | 18860.924 | |
| SNOW WATER AT START OF YEAR | 0.000 | 0.000 | 0.00 |
| SNOW WATER AT END OF YEAR | 0.000 | 0.000 | 0.00 |
| ANNUAL WATER BUDGET BALANCE | -0.0005 | -0.005 | 0.00 |
| | | | |

AVERAGE MONTHLY VALUES (MM) FOR YEARS 1923 THROUGH 2022

| PRECIPITATION | JAN/JUL | FEB/AUG | MAR/SEP | APR/OCT | MAY/NOV | JUN/DEC |
|-----------------|---------|---------|---------|---------|---------|---------|
| TOTALS | 108.32 | 125.65 | 140.77 | 121.45 | 100.17 | 120.21 |
| | 70.25 | 70.88 | 62.27 | 75.55 | 86.71 | 91.16 |
| STD. DEVIATIONS | 74.48 | 85.28 | 94.50 | 101.89 | 75.37 | 96.67 |
| | 65.33 | 74.25 | 50.54 | 56.69 | 62.89 | 65.51 |
| RUNOFF | | | | | | |
| TOTALS | 9.646 | 17.431 | 28.942 | 40.842 | 36.078 | 61.514 |
| | 27.420 | 23.472 | 10.511 | 9.473 | 6.660 | 5.595 |
| STD. DEVIATIONS | 30.329 | 33.997 | 58.412 | 78.858 | 54.374 | 84.544 |
| | 50.620 | 56.531 | 28.333 | 22.325 | 26.490 | 17.858 |

| TOTALS | 84.556 | 88.003 | 94.128 | 44.822 | | |
|-----------------------|--------------|------------|----------|-----------|---------|-------|
| | 36.960 | 47.807 | 49.769 | 83.606 | 80.318 | 81.21 |
| STD. DEVIATIONS | 38.716 | | 35.155 | | 9.155 | |
| | 5.313 | 12.660 | 22.314 | 26.858 | 42.368 | 44.59 |
| LATERAL DRAINAGE COLI | ECTED FROM | LAYER 2 | | | | |
| TOTALS | | 7.9825 | 10.0449 | 12.2253 | 14.8827 | |
| | 15.7363 | 12.9162 | 10.2361 | 9.4127 | 7.8965 | 7.53 |
| STD. DEVIATIONS | 2.0056 | | | | | |
| | 4.2016 | 4.3003 | 3.3129 | 2.7078 | 2.1489 | 1.81 |
| PERCOLATION/LEAKAGE | THROUGH LAYE | R 4 | | | | |
| TOTALS | 0.0036 | 0.0034 | 0.0040 | 0.0041 | 0.0046 | 0.00 |
| | 0.0048 | 0.0046 | 0.0042 | 0.0041 | 0.0037 | 0.00 |
| STD. DEVIATIONS | 0.0004 | 0.0005 | 0.0006 | 0.0007 | 0.0006 | 0.00 |
| | 0.0004 | 0.0004 | 0.0004 | 0.0004 | 0.0004 | 0.00 |
| PERCOLATION/LEAKAGE | THROUGH LAYE | R 6 | | | | |
| TOTALS | 0.0000 | | 0.0000 | 0.0000 | | |
| | 0.0122 | 0.0000 | 0.0000 | 0.0061 | 0.0000 | 0.03 |
| STD. DEVIATIONS | 0.0000 | 0.0608 | 0.0000 | 0.0000 | 0.0608 | 0.00 |
| | 0.0856 | 0.0000 | 0.0000 | 0.0608 | 0.0000 | 0.08 |
| AVERAG | GES OF MONTH | ILY AVERAG | ED DAILY | HEADS (CM | l) | |
| | | | | | | |
| DAILY AVERAGE HEAD ON | N TOP OF LAY | YER 3 | | | | |
| AVERAGES | 66.3632 | 70.0554 | 74.4490 | 79.7412 | 85.8644 | 90.31 |
| | 89.7337 | 85.8534 | 80.9613 | 76.9465 | 70.5300 | 67.65 |
| STD. DEVIATIONS | 7.6618 | 10.8146 | 10.8947 | 13.8571 | 11.6919 | 9.45 |
| | | | | 7.3882 | | |

AVERAGE ANNUAL TOTALS & (STD. DEVIATIONS) FOR YEARS 1923 THROUGH 2022

| | ММ | CU. METERS | PERCENT |
|--|-----------------------|------------|----------|
| PRECIPITATION | 1173.39 (283.704) | 11733.9 | 100.00 |
| RUNOFF | 277.584 (204.9355) | 2775.84 | 23.657 |
| EVAPOTRANSPIRATION | 762.906 (116.8757) | 7629.06 | 65.017 |
| LATERAL DRAINAGE COLLECTED FROM LAYER 2 | 132.87039 (20.77154) | 1328.704 | 11.32368 |
| PERCOLATION/LEAKAGE THROUGH LAYER 4 | 0.04938 (0.00295) | 0.494 | 0.00421 |
| AVERAGE HEAD ON TOP OF LAYER 3 | 782.053 (46.851) | | |
| PERCOLATION/LEAKAGE THROUGH LAYER 6 | 0.04866 (0.16584) | 0.487 | 0.00415 |
| CHANGE IN WATER STORAGE | -0.022 (1.3347) | -0.22 | -0.002 |

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PEAK DAILY VALUES FOR YEARS 1923 THROUGH 2022

| | (MM) | (CU. METERS) |
|--|-------------|--------------|
| PRECIPITATION | 150.40 | 1504.000 |
| RUNOFF | 147.975 | 1479.7485 |
| DRAINAGE COLLECTED FROM LAYER 2 | 0.79088 | 7.90884 |
| PERCOLATION/LEAKAGE THROUGH LAYER 4 | 0.000173 | 0.00173 |
| AVERAGE HEAD ON TOP OF LAYER 3 | 999.995 | |
| MAXIMUM HEAD ON TOP OF LAYER 3 | 1594.380 | |
| LOCATION OF MAXIMUM HEAD IN LAYER 2 (DISTANCE FROM DRAIN) | 16.6 METERS | |

| PERCOLATION/LEAKA | GE THROUGH LAYER | 6 | 0.608227 | 6.08227 | | | | | |
|---|-------------------|----------|-------------------|---------|--|--|--|--|--|
| SNOW WATER | | | 0.00 | 0.0000 | | | | | |
| MAXIMUM VEG. SOIL | WATER (VOL/VOL) | | 0.4413 | | | | | | |
| MINIMUM VEG. SOIL | WATER (VOL/VOL) | | 0.1227 | | | | | | |
| *** Maximum hea | ds are computed u | sing McE | nroe's equations. | *** | | | | | |
| Reference: Maximum Saturated Depth over Landfill Liner by Bruce M. McEnroe, University of Kansas ASCE Journal of Environmental Engineering Vol. 119, No. 2, March 1993, pp. 262-270. | | | | | | | | | |
| ****** | ***** | ****** | ***** | ***** | | | | | |
| | | | | | | | | | |
| ↑ ************************************ | ***** | ****** | ***** | **** | | | | | |
| FINA | L WATER STORAGE A | T END OF | YEAR 2022 | | | | | | |
| | ER (CM) | | (VOL/VOL) | | | | | | |
| 1 | 2.451 | .9 | 0.1226 | | | | | | |
| 2 | 28.003 | 6 | 0.3500 | | | | | | |
| 3 | 0.000 | 0 | 0.0000 | | | | | | |
| 4 | 0.450 | 0 | 0.7500 | | | | | | |
| 5 | 11.129 | 0 | 0.3710 | | | | | | |
| 6 | 145.951 | .0 | 0.2919 | | | | | | |
| SNOW | WATER 0.000 |) | | | | | | | |
| *************************************** | | | | | | | | | |



50th percentile year (2008)

| LANDFILL GENERATION | | |
|-------------------------------------|--------|---------|
| Daily cover | - | m2 |
| Interim cover (flat) | 46,000 | |
| Interim cover (sloped) | 20,700 | |
| Final cap - Option 1 (flat) | - | m2 |
| Final cap - Option 1 (sloped) | 40,513 | |
| Final cap - Option 2 (flat) | - | m2 |
| Final cap - Option 2 (sloped) | - | m2 |
| Centre area - Green waste | 6,300 | m2 |
| OTHER GENERATION | | |
| Open cell | 17,220 | m2 |
| Centre area - Transfer station | 11,800 | m2 |
| Transfer station infiltration rate | 3.0% | |
| STORAGE | | |
| Pond storage capacity | 1,021 | m3 |
| Freeboard storage capacity | - | m3 |
| Pond storage surface area | 900 | m2 |
| Pond storage basal area | 186 | m2 |
| Pond storage catchment area | 900 | m2 |
| Initial pond volume | 0.5 | vol/vol |
| Pan evaporation percentage - winter | 70% | |
| Pan evaporation percentage - autumn | 75% | |
| Pan evaporation percentage - spring | 70% | |
| Pan evaporation percentage - summer | 70% | |
| DISPOSAL | | |
| Pond operating volume | 0.2 | |

| Parameter | lanuary | February | March | A muli | May | June | Index | A | Contombor | October | November | December | Annua | al Total | Percent |
|---|---------|----------|-------|--------|-------|-------|-------|--------|-----------|---------|----------|---------------------------------------|-------|----------|---------|
| Parameter | January | February | | April | | | July | August | September | | | | mm | m3 | Percent |
| | 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 30 | 31 | | | |
| Precipitation (mm) | | | | | | | | | | | | | | | |
| Rainfall (2008) (mm) | 106.7 | 257.2 | 46.3 | 166.1 | 13.5 | 164.3 | 55.0 | 47.0 | 99.9 | 69.6 | 76.1 | 88.8 | 1191 | | 100% |
| Pan Evaporation | | | | | | | | | | | | | | | |
| Evaporation (from SILO) (mm) | 146.6 | 110.1 | 127.8 | 82.9 | 58.0 | 50.0 | 62.2 | 78.5 | 115.9 | 141.4 | 142.1 | 178.1 | 1294 | | 109% |
| Pan evaporation (mm) | 102.6 | 77.1 | 95.9 | 62.2 | 43.5 | 35.0 | 43.5 | 55.0 | 86.9 | 106.1 | 106.6 | 124.7 | 939 | | 79% |
| Runoff - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Interim cover (flat) | 22.0 | 66.1 | 5.1 | 39.8 | 0.1 | 41.1 | 7.0 | 4.0 | 29.4 | 5.7 | 11.6 | 19.0 | 251 | 11542 | 21% |
| Interim cover (sloped) | 21.1 | 65.9 | 4.7 | 38.7 | 0.1 | 39.9 | 6.6 | 3.7 | 28.7 | 5.3 | 10.8 | 18.5 | 244 | 0 | 21% |
| Final cap - Option 1 (flat) | 23.0 | 100.9 | 0.0 | 56.0 | 0.0 | 68.8 | 0.4 | 0.0 | 37.1 | 0.0 | 0.0 | 3.4 | 290 | 11730 | 24% |
| Final cap - Option 1 (sloped) | 25.5 | 102.5 | 0.0 | 58.8 | 0.0 | 70.3 | 0.7 | 0.0 | 38.9 | 0.0 | 0.1 | 5.1 | 302 | 12229 | 25% |
| Final cap - Option 2 (flat) | 0.0 | 119.2 | 1.1 | 26.6 | 111.3 | 91.1 | 6.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 356 | 0 | 30% |
| Final cap - Option 2 (sloped) | 0.0 | 67.1 | 0.0 | 29.3 | 0.0 | 94.6 | 0.1 | 0.0 | 48.2 | 0.0 | 0.0 | 0.7 | 240 | 0 | 20% |
| Centre area - Green waste | 35.1 | 119.9 | 0.1 | 77.5 | 0.0 | 86.2 | 2.0 | 0.2 | 51.4 | 0.4 | 1.0 | 8.5 | 382 | 2408 | 32% |
| Total Runoff (m3/month) | 2,703 | 9,311 | 334 | 5,504 | 9 | 6,107 | 500 | 262 | 3,848 | 377 | 765 | 1,516 | | 37,909 | |
| Evapotranspiration - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 37.2 | 68.4 | 38.9 | 56.2 | 10.1 | 52.2 | 18.4 | 31.6 | 39.6 | 46.1 | 29.0 | 48.8 | 476 | 0 | 40% |
| Interim cover (flat) | 50.7 | 87.0 | 61.5 | 74.2 | 20.2 | 63.8 | 21.5 | 47.2 | 49.6 | 55.0 | 47.0 | 71.2 | 649 | 29854 | 55% |
| Interim cover (sloped) | 50.6 | 84.1 | 61.0 | 71.3 | 20.4 | 63.4 | 21.8 | 46.2 | 50.4 | 53.6 | 47.8 | 69.8 | 641 | 13260 | 54% |
| Final cap - Option 1 (flat) | 72.8 | 107.4 | 72.6 | 55.0 | 34.8 | 52.6 | 30.5 | 47.7 | 66.5 | 69.6 | 54.5 | 95.8 | 760 | 0 | 64% |
| Final cap - Option 1 (sloped) | 70.7 | 106.5 | 72.1 | 54.8 | 33.3 | 51.9 | 30.2 | 46.8 | 64.1 | 69.8 | 54.5 | 94.5 | 749 | 30351 | 63% |
| Final cap - Option 2 (flat) | 77.3 | 82.7 | 139.9 | 45.7 | 42.5 | 37.3 | 38.9 | 41.6 | 15.2 | 101.3 | 70.6 | 56.7 | 750 | 0 | 63% |
| Final cap - Option 2 (sloped) | 86.4 | 131.9 | 102.4 | 33.6 | 21.6 | 30.6 | 32.2 | 49.6 | 62.6 | 103.1 | 57.8 | 100.9 | 813 | 0 | 68% |
| Centre area - Green waste | 67.8 | 106.9 | 72.4 | 55.8 | 37.5 | 53.3 | 38.6 | 56.9 | 64.7 | 67.5 | 52.6 | 94.9 | 769 | 4844 | 65% |
| Total Evapotranspiration (m3/month) | 6,671 | 10,733 | 7,469 | 7,460 | 2,935 | 6,688 | 2,909 | 5,383 | 6,329 | 6,891 | 5,693 | 9,146 | | 78,308 | |
| Leachate - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 81.6 | 100.3 | 104.6 | 60.3 | 105.2 | 63.0 | 60.0 | 29.4 | 56.4 | 46.4 | 15.4 | 51.3 | 774 | 0 | 65% |
| Interim cover (flat) | 36.7 | 57.1 | 48.4 | 13.5 | 33.3 | 40.8 | 24.3 | 4.4 | 38.3 | 4.9 | 7.0 | 13.6 | 322 | 14823 | 27% |
| Interim cover (sloped) | 27.8 | 56.6 | 53.2 | 14.3 | 33.5 | 42.2 | 21.8 | 4.4 | 37.2 | 6.4 | 5.2 | 14.2 | 317 | 6556 | 27% |
| Final cap - Option 1 (flat) | 7.7 | 21.2 | 10.8 | 7.5 | 20.9 | 15.6 | 18.1 | 15.5 | 12.4 | 6.2 | 0.6 | 6.3 | 143 | 0 | 12% |
| Final cap - Option 1 (sloped) | 8.1 | 20.3 | 10.8 | 7.1 | 20.2 | 14.8 | 17.8 | 15.6 | 12.9 | 6.8 | 0.6 | 6.0 | 141 | 5714 | 12% |
| Final cap - Option 2 (flat) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Final cap - Option 2 (sloped) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Centre area - Green waste | 2.5 | 0.0 | 3.6 | 3.7 | 4.2 | 2.0 | 2.1 | 1.6 | 2.0 | 3.2 | 6.4 | 5.2 | 36 | 230 | 3% |
| Total Leachate Collected (m3/month) | 2,607 | 4,621 | 3,788 | 1,226 | 3,071 | 3,361 | 2,303 | 937 | 3,065 | 653 | 494 | 1,196 | | 27,322 | |
| Other Leachate Sources (m3/month) | | | | | | | | | | | | · · · · · · · · · · · · · · · · · · · | | | |
| Open cell | 1,837 | 4,429 | 797 | 2,860 | 232 | 2,829 | 947 | 809 | 1,720 | 1,199 | 1,310 | 1,529 | | 20,500 | |
| Centre area - Transfer station | 38 | 91 | 16 | 59 | 5 | 58 | 19 | 17 | 35 | 25 | 27 | 31 | | 421 | |
| Leachate Storage Pond | | | | | | | | | | | | | | | |
| Rainfall into pond (m3) | 96 | 231 | 42 | 149 | 12 | 148 | 50 | 42 | 90 | 63 | 68 | 80 | | 1,071 | |
| Evaporation from pond (m3) | 56 | 69 | 86 | 56 | 39 | 32 | 39 | 49 | 78 | 95 | 96 | 112 | | 808 | |
| Net Leachate Generation (m3) | 4,522 | 9,303 | 4,557 | 4,238 | 3,281 | 6,365 | 3,279 | 1,756 | 4,832 | 1,844 | 1,804 | 2,724 | | 48,507 | |



10th percentile year (1952)

| LANDFILL GENERATION | | |
|-------------------------------------|--------|---------|
| Daily cover | - | m2 |
| Interim cover (flat) | 46,000 | m2 |
| Interim cover (sloped) | 20,700 | m2 |
| Final cap - Option 1 (flat) | - | m2 |
| Final cap - Option 1 (sloped) | 40,513 | m2 |
| Final cap - Option 2 (flat) | - | m2 |
| Final cap - Option 2 (sloped) | - | m2 |
| Centre area - Green waste | 6,300 | m2 |
| OTHER GENERATION | | |
| Open cell | 17,220 | m2 |
| Centre area - Transfer station | 11,800 | m2 |
| Transfer station infiltration rate | 3.0% | |
| STORAGE | | |
| Pond storage capacity | 1,021 | m3 |
| Freeboard storage capacity | - | m3 |
| Pond storage surface area | 900 | m2 |
| Pond storage basal area | 186 | m2 |
| Pond storage catchment area | 900 | m2 |
| Initial pond volume | 0.5 | vol/vol |
| Pan evaporation percentage - winter | 70% | |
| Pan evaporation percentage - autumn | 75% | |
| Pan evaporation percentage - spring | 70% | |
| Pan evaporation percentage - summer | 70% | |
| DISPOSAL | | |
| Pond operating volume | 0.2 | |

| Devenueden | lanuani | February | Marah | Amril | May | lune | July | August | Contombor | Ostahar | Neversher | December | Annua | I Total | Percent |
|---|---------|----------|--------|--------|-------|-------|--------|--------|-----------|---------|-----------|----------|-------|---------|---------|
| Parameter | January | February | March | April | | June | July | August | September | October | November | December | mm | m3 | Percent |
| | 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 30 | 31 | | | |
| Precipitation (mm) | | | | | _ | | | | | | | | | | |
| Rainfall (1952) (mm) | 46.4 | 28.0 | 228.0 | 320.7 | 45.6 | 111.4 | 317.4 | 371.3 | 24.4 | 115.1 | 43.1 | 50.1 | 1702 | | 100% |
| Pan Evaporation | | | | | | | | | | | | | | | |
| Evaporation (from SILO) (mm) | 170.9 | 139.6 | 120.8 | 91.2 | 66.9 | 55.3 | 63.6 | 89.2 | 115.9 | 143.4 | 157.6 | 181.5 | 1396 | | 82% |
| Pan evaporation (mm) | 119.6 | 97.7 | 90.6 | 68.4 | 50.2 | 38.7 | 44.5 | 62.4 | 86.9 | 107.6 | 118.2 | 127.1 | 1012 | | 59% |
| Runoff - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Interim cover (flat) | 9.1 | 1.3 | 79.3 | 88.2 | 2.6 | 35.0 | 131.0 | 132.7 | 0.6 | 19.4 | 1.7 | 1.8 | 503 | 23121 | 30% |
| Interim cover (sloped) | 9.5 | 1.4 | 80.4 | 90.7 | 2.8 | 35.7 | 131.9 | 134.7 | 0.7 | 20.4 | 1.9 | 1.8 | 512 | 10594 | 30% |
| Final cap - Option 1 (flat) | 0.6 | 0.0 | 116.8 | 188.1 | 0.0 | 46.6 | 244.0 | 305.6 | 0.0 | 2.7 | 0.0 | 0.0 | 904 | 0 | 53% |
| Final cap - Option 1 (sloped) | 1.1 | 0.0 | 120.5 | 188.5 | 0.0 | 48.5 | 246.4 | 305.5 | 0.0 | 4.1 | 0.0 | 0.0 | 915 | 37052 | 54% |
| Final cap - Option 2 (flat) | 0.0 | 0.0 | 73.0 | 222.0 | 9.3 | 65.1 | 257.4 | 322.1 | 0.0 | 3.5 | 0.0 | 0.0 | 952 | 0 | 56% |
| Final cap - Option 2 (sloped) | 0.0 | 0.0 | 58.4 | 195.8 | 0.2 | 51.3 | 243.6 | 310.4 | 0.0 | 0.9 | 0.0 | 0.0 | 861 | 0 | 51% |
| Centre area - Green waste | 3.1 | 0.0 | 125.1 | 216.0 | 4.5 | 60.2 | 257.4 | 320.9 | 0.0 | 14.4 | 0.0 | 0.0 | 1002 | 6310 | 59% |
| Total Runoff (m3/month) | 677 | 86 | 10,979 | 14,934 | 206 | 4,693 | 20,361 | 23,294 | 39 | 1,571 | 116 | 118 | | 77,075 | |
| Evapotranspiration - Calculated using HELP (mm) | | | | - | - | | | - | | | - | - | - | | |
| Daily cover | 20.0 | 8.3 | 44.4 | 77.5 | 41.0 | 18.3 | 19.5 | 56.7 | 9.9 | 63.3 | 30.6 | 30.2 | 420 | 0 | 25% |
| Interim cover (flat) | 34.8 | 7.5 | 62.1 | 89.7 | 65.2 | 32.6 | 18.7 | 73.7 | 9.1 | 83.3 | 34.1 | 38.1 | 549 | 25247 | 32% |
| Interim cover (sloped) | 34.6 | 7.5 | 62.1 | 89.2 | 64.6 | 32.5 | 18.7 | 73.4 | 9.1 | 83.0 | 26.9 | 41.7 | 543 | 11247 | 32% |
| Final cap - Option 1 (flat) | 41.0 | 27.8 | 82.5 | 77.5 | 55.7 | 35.3 | 34.2 | 69.2 | 23.2 | 99.2 | 50.9 | 41.8 | 638 | 0 | 38% |
| Final cap - Option 1 (sloped) | 40.6 | 27.8 | 82.7 | 73.4 | 55.4 | 34.6 | 33.3 | 68.7 | 22.1 | 98.3 | 50.6 | 41.8 | 629 | 25493 | 37% |
| Final cap - Option 2 (flat) | 46.4 | 27.8 | 81.6 | 71.7 | 48.2 | 43.1 | 43.8 | 67.5 | 35.7 | 115.2 | 93.8 | 42.3 | 717 | 0 | 42% |
| Final cap - Option 2 (sloped) | 46.4 | 27.7 | 81.5 | 67.3 | 48.7 | 43.0 | 41.4 | 66.6 | 35.8 | 114.8 | 71.1 | 42.3 | 686 | 0 | 40% |
| Centre area - Green waste | 41.5 | 27.6 | 82.6 | 78.8 | 57.3 | 45.2 | 39.5 | 70.1 | 22.1 | 98.3 | 53.7 | 42.2 | 659 | 4151 | 39% |
| Total Evapotranspiration (m3/month) | 4,221 | 1,804 | 8,014 | 9,438 | 6,942 | 3,860 | 2,845 | 8,134 | 1,643 | 10,146 | 4,516 | 4,574 | | 66,138 | |
| Leachate - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 58.1 | 4.2 | 26.0 | 147.2 | 173.1 | 97.2 | 94.9 | 364.1 | 174.9 | 83.7 | 67.6 | 10.9 | 1302 | 0 | 77% |
| Interim cover (flat) | 3.0 | 0.0 | 18.5 | 67.7 | 103.8 | 50.1 | 32.1 | 144.2 | 140.9 | 65.7 | 3.4 | 0.0 | 629 | 28946 | 37% |
| Interim cover (sloped) | 2.2 | 0.0 | 18.0 | 67.7 | 103.0 | 49.3 | 30.9 | 142.2 | 140.3 | 63.5 | 2.2 | 5.2 | 624 | 12925 | 37% |
| Final cap - Option 1 (flat) | 8.1 | 0.0 | 0.0 | 24.5 | 29.6 | 16.5 | 18.0 | 24.9 | 15.0 | 7.3 | 8.2 | 0.0 | 152 | 0 | 9% |
| Final cap - Option 1 (sloped) | 8.0 | 0.0 | 0.0 | 24.2 | 29.8 | 16.3 | 17.1 | 25.6 | 14.8 | 6.7 | 8.6 | 0.0 | 151 | 6121 | 9% |
| Final cap - Option 2 (flat) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Final cap - Option 2 (sloped) | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Centre area - Green waste | 3.5 | 1.9 | | | | | | 1.4 | 1.6 | | 4.1 | 5.1 | 34 | 216 | 2% |
| Total Leachate Collected (m3/month) | 532 | 12 | 1,245 | 5,508 | 8,115 | 4,008 | 2,808 | 10,622 | 9,994 | 4,647 | 577 | 140 | | 48,209 | |
| Other Leachate Sources (m3/month) | | | | | | | | | | | | | | | |
| Open cell | 799 | 482 | 3,926 | 5,522 | 785 | 1,918 | 5,466 | 6,394 | 420 | 1,982 | 742 | 863 | | 29,300 | |
| Centre area - Transfer station | 16 | 10 | 81 | 114 | 16 | 39 | 112 | 131 | 9 | 41 | 15 | 18 | | 602 | |
| Leachate Storage Pond | | | | | | | | | | | | | | | |
| Rainfall into pond (m3) | 42 | 25 | 205 | 289 | 41 | 100 | 286 | 334 | 22 | 104 | 39 | 45 | | 1,531 | |
| Evaporation from pond (m3) | 65 | 88 | 82 | 62 | 45 | 35 | 40 | 56 | 78 | 97 | 106 | 114 | | 868 | |
| Net Leachate Generation (m3) | 1,324 | 441 | 5,376 | 11,371 | 8,913 | 6,032 | 8,632 | 17,425 | 10,367 | 6,677 | 1,267 | 951 | | 78,774 | |





50th percentile year (2008)

| LANDFILL GENERATION | | - |
|-------------------------------------|--------|---------|
| Daily cover | 600 | |
| Interim cover (flat) | 46,000 | |
| Interim cover (sloped) | 27,133 | |
| Final cap - Option 1 (flat) | - | m2 |
| Final cap - Option 1 (sloped) | 28,062 | |
| Final cap - Option 2 (flat) | - | m2 |
| Final cap - Option 2 (sloped) | 10,187 | |
| Centre area - Green waste | 6,300 | m2 |
| OTHER GENERATION | | |
| Open cell | 21,319 | m2 |
| Centre area - Transfer station | 11,800 | m2 |
| Transfer station infiltration rate | 3.0% | |
| STORAGE | | |
| Pond storage capacity | 1,021 | m3 |
| Freeboard storage capacity | - | m3 |
| Pond storage surface area | 900 | m2 |
| Pond storage basal area | 186 | m2 |
| Pond storage catchment area | 900 | m2 |
| Initial pond volume | 0.5 | vol/vol |
| Pan evaporation percentage - winter | 70% | |
| Pan evaporation percentage - autumn | 75% | |
| Pan evaporation percentage - spring | 70% | |
| Pan evaporation percentage - summer | 70% | |
| DISPOSAL | | |
| Pond operating volume | 0.2 | |

| Parameter | lanuaru | February | March | المستا | Mari | June | Index | A | Contombor | October | November | December | Annua | I Total | Percent |
|---|---------|----------|-------|--------|-------|-------|-------|--------|-----------|---------|----------|----------|-------|---------|---------|
| Parameter | January | February | | April | Мау | | July | August | September | October | | | mm | m3 | Percent |
| | 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 30 | 31 | | | |
| Precipitation (mm) | | | | | | | | | | | | | | | |
| Rainfall (2008) (mm) | 106.7 | 257.2 | 46.3 | 166.1 | 13.5 | 164.3 | 55.0 | 47.0 | 99.9 | 69.6 | 76.1 | 88.8 | 1191 | | 100% |
| Pan Evaporation | | | | | | | | | | | | | | | |
| Evaporation (from SILO) (mm) | 146.6 | 110.1 | 127.8 | 82.9 | 58.0 | 50.0 | 62.2 | 78.5 | 115.9 | 141.4 | 142.1 | 178.1 | 1294 | | 109% |
| Pan evaporation (mm) | 102.6 | 77.1 | 95.9 | 62.2 | 43.5 | 35.0 | 43.5 | 55.0 | 86.9 | 106.1 | 106.6 | 124.7 | 939 | | 79% |
| Runoff - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Interim cover (flat) | 22.0 | 66.1 | 5.1 | 39.8 | 0.1 | 41.1 | 7.0 | 4.0 | 29.4 | 5.7 | 11.6 | 19.0 | 251 | 11542 | 21% |
| Interim cover (sloped) | 21.1 | 65.9 | 4.7 | 38.7 | 0.1 | 39.9 | 6.6 | 3.7 | 28.7 | 5.3 | 10.8 | 18.5 | 244 | 0 | 21% |
| Final cap - Option 1 (flat) | 23.0 | 100.9 | 0.0 | 56.0 | 0.0 | 68.8 | 0.4 | 0.0 | 37.1 | 0.0 | 0.0 | 3.4 | 290 | 8125 | 24% |
| Final cap - Option 1 (sloped) | 25.5 | 102.5 | 0.0 | 58.8 | 0.0 | 70.3 | 0.7 | 0.0 | 38.9 | 0.0 | 0.1 | 5.1 | 302 | 8471 | 25% |
| Final cap - Option 2 (flat) | 0.0 | 119.2 | 1.1 | 26.6 | 111.3 | 91.1 | 6.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 356 | 0 | 30% |
| Final cap - Option 2 (sloped) | 0.0 | 67.1 | 0.0 | 29.3 | 0.0 | 94.6 | 0.1 | 0.0 | 48.2 | 0.0 | 0.0 | 0.7 | 240 | 2447 | 20% |
| Centre area - Green waste | 35.1 | 119.9 | 0.1 | 77.5 | 0.0 | 86.2 | 2.0 | 0.2 | 51.4 | 0.4 | 1.0 | 8.5 | 382 | 2408 | 32% |
| Total Runoff (m3/month) | 2,521 | 9,143 | 364 | 5,320 | 9 | 6,453 | 535 | 286 | 4,040 | 411 | 834 | 1,580 | | 32,992 | |
| Evapotranspiration - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 37.2 | 68.4 | 38.9 | 56.2 | 10.1 | 52.2 | 18.4 | 31.6 | 39.6 | 46.1 | 29.0 | 48.8 | 476 | 286 | 40% |
| Interim cover (flat) | 50.7 | 87.0 | 61.5 | 74.2 | 20.2 | 63.8 | 21.5 | 47.2 | 49.6 | 55.0 | 47.0 | 71.2 | 649 | 29854 | 55% |
| Interim cover (sloped) | 50.6 | 84.1 | 61.0 | 71.3 | 20.4 | 63.4 | 21.8 | 46.2 | 50.4 | 53.6 | 47.8 | 69.8 | 641 | 17381 | 54% |
| Final cap - Option 1 (flat) | 72.8 | 107.4 | 72.6 | 55.0 | 34.8 | 52.6 | 30.5 | 47.7 | 66.5 | 69.6 | 54.5 | 95.8 | 760 | 0 | 64% |
| Final cap - Option 1 (sloped) | 70.7 | 106.5 | 72.1 | 54.8 | 33.3 | 51.9 | 30.2 | 46.8 | 64.1 | 69.8 | 54.5 | 94.5 | 749 | 21023 | 63% |
| Final cap - Option 2 (flat) | 77.3 | 82.7 | 139.9 | 45.7 | 42.5 | 37.3 | 38.9 | 41.6 | 15.2 | 101.3 | 70.6 | 56.7 | 750 | 0 | 63% |
| Final cap - Option 2 (sloped) | 86.4 | 131.9 | 102.4 | 33.6 | 21.6 | 30.6 | 32.2 | 49.6 | 62.6 | 103.1 | 57.8 | 100.9 | 813 | 8279 | 68% |
| Centre area - Green waste | 67.8 | 106.9 | 72.4 | 55.8 | 37.5 | 53.3 | 38.6 | 56.9 | 64.7 | 67.5 | 52.6 | 94.9 | 769 | 4844 | 65% |
| Total Evapotranspiration (m3/month) | 7,019 | 11,333 | 8,030 | 7,612 | 2,879 | 6,792 | 3,013 | 5,621 | 6,517 | 7,446 | 5,928 | 9,476 | | 81,666 | |
| Leachate - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 81.6 | 100.3 | 104.6 | 60.3 | 105.2 | 63.0 | 60.0 | 29.4 | 56.4 | 46.4 | 15.4 | 51.3 | 774 | 464 | 65% |
| Interim cover (flat) | 36.7 | 57.1 | 48.4 | 13.5 | 33.3 | 40.8 | 24.3 | 4.4 | 38.3 | 4.9 | 7.0 | 13.6 | 322 | 14823 | 27% |
| Interim cover (sloped) | 27.8 | 56.6 | 53.2 | 14.3 | 33.5 | 42.2 | 21.8 | 4.4 | 37.2 | 6.4 | 5.2 | 14.2 | 317 | 8593 | 27% |
| Final cap - Option 1 (flat) | 7.7 | 21.2 | 10.8 | 7.5 | 20.9 | 15.6 | 18.1 | 15.5 | 12.4 | 6.2 | 0.6 | 6.3 | 143 | 0 | 12% |
| Final cap - Option 1 (sloped) | 8.1 | 20.3 | 10.8 | 7.1 | 20.2 | 14.8 | 17.8 | 15.6 | 12.9 | 6.8 | 0.6 | 6.0 | 141 | 3958 | 12% |
| Final cap - Option 2 (flat) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Final cap - Option 2 (sloped) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Centre area - Green waste | 2.5 | 0.0 | 3.6 | 3.7 | 4.2 | 2.0 | 2.1 | 1.6 | 2.0 | 3.2 | 6.4 | 5.2 | 36 | 230 | 3% |
| Total Leachate Collected (m3/month) | 2,734 | 4,792 | 4,059 | 1,266 | 3,097 | 3,486 | 2,256 | 789 | 3,178 | 638 | 529 | 1,244 | | 28,068 | |
| Other Leachate Sources (m3/month) | | | | | | | | | | | | | | | |
| Open cell | 2,275 | 5,483 | 987 | 3,541 | 288 | 3,503 | 1,173 | 1,002 | 2,130 | 1,484 | 1,622 | 1,893 | | 25,380 | |
| Centre area - Transfer station | 38 | 91 | 16 | 59 | 5 | 58 | 19 | 17 | 35 | 25 | 27 | 31 | | 421 | |
| Leachate Storage Pond | | | | | | | | | | | | | | | |
| Rainfall into pond (m3) | 96 | 231 | 42 | 149 | 12 | 148 | 50 | 42 | 90 | 63 | 68 | 80 | | 1,071 | |
| Evaporation from pond (m3) | 56 | 69 | 86 | 56 | 39 | 32 | 39 | 49 | 78 | 95 | 96 | 112 | | 808 | |
| Net Leachate Generation (m3) | 5,087 | 10,528 | 5,018 | 4,959 | 3,363 | 7,164 | 3,459 | 1,801 | 5,355 | 2,113 | 2,150 | 3,136 | | 54,133 | |



10th percentile year (1952)

| LANDFILL GENERATION | | |
|-------------------------------------|--------|---------|
| Daily cover | 600 | m2 |
| Interim cover (flat) | 46,000 | |
| Interim cover (sloped) | 27,133 | m2 |
| Final cap - Option 1 (flat) | - | m2 |
| Final cap - Option 1 (sloped) | 28,062 | |
| Final cap - Option 2 (flat) | - | m2 |
| Final cap - Option 2 (sloped) | 10,187 | |
| Centre area - Green waste | 6,300 | m2 |
| OTHER GENERATION | | |
| Open cell | 21,319 | m2 |
| Centre area - Transfer station | 11,800 | m2 |
| Transfer station infiltration rate | 3.0% | |
| STORAGE | | |
| Pond storage capacity | 1,021 | m3 |
| Freeboard storage capacity | - | m3 |
| Pond storage surface area | 900 | m2 |
| Pond storage basal area | 186 | m2 |
| Pond storage catchment area | 900 | m2 |
| Initial pond volume | 0.5 | vol/vol |
| Pan evaporation percentage - winter | 70% | |
| Pan evaporation percentage - autumn | 75% | |
| Pan evaporation percentage - spring | 70% | |
| Pan evaporation percentage - summer | 70% | |
| DISPOSAL | | |
| Pond operating volume | 0.2 | |

| Parameter | January | February | March | April | Мау | June | July | August | September | October | November | December | Annua | l Total | Percent |
|--|---------------|--------------|--------------|---------------|--------------|---------------|---------------|---------------|--------------|---------------|---------------|--------------|------------|----------------|------------|
| Falanetei | | | | - | - | | - | - | - | | | | mm | m3 | Fercent |
| | 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 30 | 31 | | | |
| Precipitation (mm) | | - | | | | | | | | | - | - | | | |
| Rainfall (1952) (mm) | 46.4 | 28.0 | 228.0 | 320.7 | 45.6 | 111.4 | 317.4 | 371.3 | 24.4 | 115.1 | 43.1 | 50.1 | 1702 | | 100% |
| Pan Evaporation | | - | | | | | | | | | - | - | | | |
| Evaporation (from SILO) (mm) | 170.9 | 139.6 | 120.8 | 91.2 | 66.9 | 55.3 | 63.6 | 89.2 | 115.9 | 143.4 | 157.6 | 181.5 | 1396 | | 82% |
| Pan evaporation (mm) | 119.6 | 97.7 | 90.6 | 68.4 | 50.2 | 38.7 | 44.5 | 62.4 | 86.9 | 107.6 | 118.2 | 127.1 | 1012 | | 59% |
| Runoff - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Interim cover (flat) | 9.1 | 1.3 | 79.3 | 88.2 | 2.6 | 35.0 | 131.0 | 132.7 | 0.6 | 19.4 | 1.7 | 1.8 | 503 | 23121 | 30% |
| Interim cover (sloped) | 9.5 | 1.4 | 80.4 | 90.7 | 2.8 | 35.7 | 131.9 | 134.7 | 0.7 | 20.4 | 1.9 | 1.8 | 512 | 13886 | 30% |
| Final cap - Option 1 (flat) | 0.6 | 0.0 | 116.8 | 188.1 | 0.0 | 46.6 | 244.0 | 305.6 | 0.0 | 2.7 | 0.0 | 0.0 | 904 | 0 | 53% |
| Final cap - Option 1 (sloped) | 1.1 | 0.0 | 120.5 | 188.5 | 0.0 | 48.5 | 246.4 | 305.5 | 0.0 | 4.1 | 0.0 | 0.0 | 915 | 25664 | 54% |
| Final cap - Option 2 (flat) | 0.0 | 0.0 | 73.0 | 222.0 | 9.3 | 65.1 | 257.4 | 322.1 | 0.0 | 3.5 | 0.0 | 0.0 | 952 | 0 | 56% |
| Final cap - Option 2 (sloped) | 0.0 | 0.0 | 58.4 | 195.8 | 0.2 | 51.3 | 243.6 | 310.4 | 0.0 | 0.9 | 0.0 | 0.0 | 861 | 8766 | 51% |
| Centre area - Green waste | 3.1 | 0.0 | 125.1 | 216.0 | 4.5 | 60.2 | 257.4 | 320.9 | 0.0 | 14.4 | 0.0 | 0.0 | 1002 | 6310 | 59% |
| Total Runoff (m3/month) | 725 | 95 | 10,591 | 15,165 | 226 | 4,841 | 20,622 | 23,518 | 43 | 1,661 | 128 | 130 | | 77,747 | |
| Evapotranspiration - Calculated using HELP (mm) | | | | | | 12.5 | | | | | | | 12.5 | | |
| Daily cover | 20.0 | 8.3 | 44.4 | 77.5 | 41.0 | 18.3 | 19.5 | 56.7 | 9.9 | 63.3 | 30.6 | 30.2 | 420 | 252 | 25% |
| Interim cover (flat) | 34.8 | 7.5 | 62.1 | 89.7 | 65.2 | 32.6 | 18.7 | 73.7 | 9.1 | 83.3 | 34.1 | 38.1 | 549 | 25247 | 32% |
| Interim cover (sloped) | 34.6 | 7.5 | 62.1 | 89.2 | 64.6 | 32.5 | 18.7 | 73.4 | 9.1 | 83.0 | 26.9 | 41.7 | 543 | 14742 | 32% |
| Final cap - Option 1 (flat) | 41.0 | 27.8 | 82.5 | 77.5 | 55.7 | 35.3 | 34.2 | 69.2 | 23.2 | 99.2 | 50.9 | 41.8 | 638 | 0 | 38% |
| Final cap - Option 1 (sloped) | 40.6 46.4 | 27.8 | 82.7 | 73.4 | 55.4 | 34.6 43.1 | 33.3 | 68.7 | 22.1 | 98.3 | 50.6 | 41.8 | 629 | 17658 | 37% |
| Final cap - Option 2 (flat) | 46.4 | 27.8 27.7 | 81.6 81.5 | 71.7 67.3 | 48.2 48.7 | 43.1 | 43.8 | 67.5 66.6 | 35.7 35.8 | 115.2 | 93.8 71.1 | 42.3 42.3 | 717 686 | 0 6992 | 42% 40% |
| Final cap - Option 2 (sloped) | | 27.6 | 81.5 | | 48.7 | 43.0 | 41.4 39.5 | | 22.1 | 114.8 98.3 | 53.7 | 42.3 | | | 40% 39% |
| Centre area - Green waste | 41.5 4,423 | | 82.6 | 78.8 9,830 | | 45.2 4,088 | 39.5 2,984 | 70.1 8,464 | 1,796 | 98.3 | 53.7 4,801 | | 659 | 4151 69,042 | 39% |
| Total Evapotranspiration (m3/month) | 4,423 | 1,793 | 0,241 | 9,030 | 7,187 | 4,000 | 2,904 | 0,404 | 1,796 | 10,664 | 4,001 | 4,771 | | 69,042 | |
| Leachate - Calculated using HELP (mm) | 58.1 | 4.2 | 26.0 | 147.2 | 173.1 | 97.2 | 94.9 | 364.1 | 174.9 | 83.7 | 67.6 | 10.9 | 1302 | 781 | 77% |
| Daily cover | 3.0 | 4.2 | 18.5 | 67.7 | 103.8 | 97.2 50.1 | 32.1 | 144.2 | 174.9 | 65.7 | 3.4 | 0.0 | 629 | 28946 | 37% |
| Interim cover (flat) Interim cover (sloped) | 3.0 | 0.0 | 18.5 | 67.7 | 103.8 | 49.3 | 32.1 | 144.2 | 140.9 | 63.5 | 3.4 | 5.2 | 629 | 28946 | 37% |
| Final cap - Option 1 (flat) | 8.1 | 0.0 | 0.0 | 24.5 | 29.6 | 49.3 | 30.9 | 24.9 | 140.3 | 7.3 | 8.2 | 5.2 0.0 | 624 152 | 0 | 37% 9% |
| Final cap - Option 1 (flat) Final cap - Option 1 (sloped) | 8.1 | 0.0 | 0.0 | 24.5 | 29.6 | 16.5 | 18.0 | 24.9 | 15.0 | 6.7 | 8.2 | 0.0 | 152 | 4240 | 9% |
| Final cap - Option 1 (sloped) Final cap - Option 2 (flat) | 0.0 | 0.0 | 0.0 | 0.0 | 29.8 | 0.0 | 0.0 | 25.6 | 0.0 | 0.0 | 0.0 | 0.0 | 151 | 4240 | 9% |
| Final cap - Option 2 (hat) Final cap - Option 2 (sloped) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Centre area - Green waste | 3.5 | 1.9 | 3.5 | 2.4 | 0.0 | 4.0 | 0.0 | 1.4 | 1.6 | 6.3 | 4.1 | 5.1 | 34 | 216 | 2% |
| | | 1.9 | 1,377 | | 8,511 | | | 11.437 | 10,818 | | 524 | 179 | 34 | 51,125 | 2 70 |
| Total Leachate Collected (m3/month) | 480 | 15 | 1,3// | 5,731 | 0,511 | 4,181 | 2,851 | 11,437 | 10,818 | 5,022 | 524 | 179 | | 51,125 | |
| Other Leachate Sources (m3/month) | 989 | 597 | 4,861 | 6,837 | 972 | 2.275 | 6,767 | 7,916 | 520 | 2,454 | 919 | 1,068 | | 36,274 | |
| Open cell | 989 | 597 10 | 4,861 | | 972 | 2,375 39 | 112 | 131 | 520 9 | 2,454 | 15 | 1,068 | | 602 | |
| Centre area - Transfer station | 10 | 10 | 81 | 114 | 16 | 39 | 112 | 131 | 9 | 41 | 15 | 18 | | 602 | |
| Leachate Storage Pond Rainfall into pond (m3) | 42 | 25 | 205 | 289 | 41 | 100 | 286 | 334 | 22 | 104 | 39 | 45 | | 1.531 | |
| | | | | | | | | | | 97 | | | | | L |
| Evaporation from pond (m3) | 65 1.463 | 88 559 | 82 6.442 | 62 12.908 | 45 9.495 | 35 6.661 | 40 9.975 | 56 19.762 | 78 11.290 | 7.523 | 106 1.391 | 114 1.196 | | 868 88.665 | |
| Net Leachate Generation (m3) | 1,463 | 559 | 6,442 | 12,908 | 9,495 | 6,661 | 9,975 | 19,762 | 11,290 | 7,523 | 1,391 | 1,196 | | 88,665 | |





50th percentile year (2008)

| LANDFILL GENERATION | | |
|-------------------------------------|--------|---------|
| Daily cover | - | m2 |
| Interim cover (flat) | 46,000 | m2 |
| Interim cover (sloped) | 20,700 | m2 |
| Final cap - Option 1 (flat) | - | m2 |
| Final cap - Option 1 (sloped) | 28,062 | |
| Final cap - Option 2 (flat) | 15,901 | |
| Final cap - Option 2 (sloped) | 22,638 | |
| Centre area - Green waste | 6,300 | m2 |
| OTHER GENERATION | | |
| Open cell | - | m2 |
| Centre area - Transfer station | 11,800 | m2 |
| Transfer station infiltration rate | 3.0% | |
| STORAGE | | |
| Pond storage capacity | 1,021 | m3 |
| Freeboard storage capacity | - | m3 |
| Pond storage surface area | 900 | m2 |
| Pond storage basal area | 186 | m2 |
| Pond storage catchment area | 900 | m2 |
| Initial pond volume | 0.5 | vol/vol |
| Pan evaporation percentage - winter | 70% | |
| Pan evaporation percentage - autumn | 75% | |
| Pan evaporation percentage - spring | 70% | |
| Pan evaporation percentage - summer | 70% | |
| DISPOSAL | | |
| Pond operating volume | 0.2 | |

| Parameter | lonuoni | February | March | April | May | June | July | August | September | October | November | December | Annua | I Total | Percent |
|---|---------|----------|--------|-------|-------|-------|-------|--------|-----------|---------|----------|----------|-------|---------|---------|
| Parameter | January | | | • | | | | | - | | | | mm | m3 | Percent |
| | 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 30 | 31 | | | |
| Precipitation (mm) | | | | | | | | | | | | | | | |
| Rainfall (2008) (mm) | 106.7 | 257.2 | 46.3 | 166.1 | 13.5 | 164.3 | 55.0 | 47.0 | 99.9 | 69.6 | 76.1 | 88.8 | 1191 | | 100% |
| Pan Evaporation | | | | | | | | | | | | | | | |
| Evaporation (from SILO) (mm) | 146.6 | 110.1 | 127.8 | 82.9 | 58.0 | 50.0 | 62.2 | 78.5 | 115.9 | 141.4 | 142.1 | 178.1 | 1294 | | 109% |
| Pan evaporation (mm) | 102.6 | 77.1 | 95.9 | 62.2 | 43.5 | 35.0 | 43.5 | 55.0 | 86.9 | 106.1 | 106.6 | 124.7 | 939 | | 79% |
| Runoff - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Interim cover (flat) | 22.0 | 66.1 | 5.1 | 39.8 | 0.1 | 41.1 | 7.0 | 4.0 | 29.4 | 5.7 | 11.6 | 19.0 | 251 | 11542 | 21% |
| Interim cover (sloped) | 21.1 | 65.9 | 4.7 | 38.7 | 0.1 | 39.9 | 6.6 | 3.7 | 28.7 | 5.3 | 10.8 | 18.5 | 244 | 0 | 21% |
| Final cap - Option 1 (flat) | 23.0 | 100.9 | 0.0 | 56.0 | 0.0 | 68.8 | 0.4 | 0.0 | 37.1 | 0.0 | 0.0 | 3.4 | 290 | 8125 | 24% |
| Final cap - Option 1 (sloped) | 25.5 | 102.5 | 0.0 | 58.8 | 0.0 | 70.3 | 0.7 | 0.0 | 38.9 | 0.0 | 0.1 | 5.1 | 302 | 8471 | 25% |
| Final cap - Option 2 (flat) | 0.0 | 119.2 | 1.1 | 26.6 | 111.3 | 91.1 | 6.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 356 | 5653 | 30% |
| Final cap - Option 2 (sloped) | 0.0 | 67.1 | 0.0 | 29.3 | 0.0 | 94.6 | 0.1 | 0.0 | 48.2 | 0.0 | 0.0 | 0.7 | 240 | 5437 | 20% |
| Centre area - Green waste | 35.1 | 119.9 | 0.1 | 77.5 | 0.0 | 86.2 | 2.0 | 0.2 | 51.4 | 0.4 | 1.0 | 8.5 | 382 | 2408 | 32% |
| Total Runoff (m3/month) | 2,386 | 11,449 | 351 | 5,859 | 1,779 | 8,823 | 592 | 262 | 4,455 | 378 | 764 | 1,470 | | 41,635 | |
| Evapotranspiration - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 37.2 | 68.4 | 38.9 | 56.2 | 10.1 | 52.2 | 18.4 | 31.6 | 39.6 | 46.1 | 29.0 | 48.8 | 476 | 0 | 40% |
| Interim cover (flat) | 50.7 | 87.0 | 61.5 | 74.2 | 20.2 | 63.8 | 21.5 | 47.2 | 49.6 | 55.0 | 47.0 | 71.2 | 649 | 29854 | 55% |
| Interim cover (sloped) | 50.6 | 84.1 | 61.0 | 71.3 | 20.4 | 63.4 | 21.8 | 46.2 | 50.4 | 53.6 | 47.8 | 69.8 | 641 | 13260 | 54% |
| Final cap - Option 1 (flat) | 72.8 | 107.4 | 72.6 | 55.0 | 34.8 | 52.6 | 30.5 | 47.7 | 66.5 | 69.6 | 54.5 | 95.8 | 760 | 0 | 64% |
| Final cap - Option 1 (sloped) | 70.7 | 106.5 | 72.1 | 54.8 | 33.3 | 51.9 | 30.2 | 46.8 | 64.1 | 69.8 | 54.5 | 94.5 | 749 | 21023 | 63% |
| Final cap - Option 2 (flat) | 77.3 | 82.7 | 139.9 | 45.7 | 42.5 | 37.3 | 38.9 | 41.6 | 15.2 | 101.3 | 70.6 | 56.7 | 750 | 11918 | 63% |
| Final cap - Option 2 (sloped) | 86.4 | 131.9 | 102.4 | 33.6 | 21.6 | 30.6 | 32.2 | 49.6 | 62.6 | 103.1 | 57.8 | 100.9 | 813 | 18399 | 68% |
| Centre area - Green waste | 67.8 | 106.9 | 72.4 | 55.8 | 37.5 | 53.3 | 38.6 | 56.9 | 64.7 | 67.5 | 52.6 | 94.9 | 769 | 4844 | 65% |
| Total Evapotranspiration (m3/month) | 8,975 | 13,707 | 11,115 | 8,265 | 3,687 | 7,326 | 3,880 | 6,583 | 7,190 | 9,968 | 7,445 | 11,156 | | 99,297 | |
| Leachate - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 81.6 | 100.3 | 104.6 | 60.3 | 105.2 | 63.0 | 60.0 | 29.4 | 56.4 | 46.4 | 15.4 | 51.3 | 774 | 0 | 65% |
| Interim cover (flat) | 36.7 | 57.1 | 48.4 | 13.5 | 33.3 | 40.8 | 24.3 | 4.4 | 38.3 | 4.9 | 7.0 | 13.6 | 322 | 14823 | 27% |
| Interim cover (sloped) | 27.8 | 56.6 | 53.2 | 14.3 | 33.5 | 42.2 | 21.8 | 4.4 | 37.2 | 6.4 | 5.2 | 14.2 | 317 | 6556 | 27% |
| Final cap - Option 1 (flat) | 7.7 | 21.2 | 10.8 | 7.5 | 20.9 | 15.6 | 18.1 | 15.5 | 12.4 | 6.2 | 0.6 | 6.3 | 143 | 0 | 12% |
| Final cap - Option 1 (sloped) | 8.1 | 20.3 | 10.8 | 7.1 | 20.2 | 14.8 | 17.8 | 15.6 | 12.9 | 6.8 | 0.6 | 6.0 | 141 | 3958 | 12% |
| Final cap - Option 2 (flat) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Final cap - Option 2 (sloped) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Centre area - Green waste | 2.5 | 0.0 | 3.6 | 3.7 | 4.2 | 2.0 | 2.1 | 1.6 | 2.0 | 3.2 | 6.4 | 5.2 | 36 | 230 | 3% |
| Total Leachate Collected (m3/month) | 2,506 | 4,368 | 3,654 | 1,138 | 2,819 | 3,177 | 2,080 | 743 | 2,905 | 569 | 486 | 1,122 | | 25,566 | |
| Other Leachate Sources (m3/month) | | | | | | | | | | | | | | | |
| Open cell | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | |
| Centre area - Transfer station | 38 | 91 | 16 | 59 | 5 | 58 | 19 | 17 | 35 | 25 | 27 | 31 | | 421 | |
| Leachate Storage Pond | | | | | | | | | | | | | | | |
| Rainfall into pond (m3) | 96 | 231 | 42 | 149 | 12 | 148 | 50 | 42 | 90 | 63 | 68 | 80 | | 1,071 | |
| Evaporation from pond (m3) | 56 | 69 | 86 | 56 | 39 | 32 | 39 | 49 | 78 | 95 | 96 | 112 | | 808 | |
| Net Leachate Generation (m3) | 2,584 | 4,621 | 3,626 | 1,290 | 2,797 | 3,352 | 2,110 | 753 | 2,952 | 560 | 485 | 1,121 | | 26,251 | |



10th percentile year (1952)

| LANDFILL GENERATION | | |
|-------------------------------------|--------|---------|
| Daily cover | - | m2 |
| Interim cover (flat) | 46,000 | m2 |
| Interim cover (sloped) | 20,700 | m2 |
| Final cap - Option 1 (flat) | - | m2 |
| Final cap - Option 1 (sloped) | 28,062 | |
| Final cap - Option 2 (flat) | 15,901 | |
| Final cap - Option 2 (sloped) | 22,638 | |
| Centre area - Green waste | 6,300 | m2 |
| OTHER GENERATION | | |
| Open cell | - | m2 |
| Centre area - Transfer station | 11,800 | m2 |
| Transfer station infiltration rate | 3.0% | |
| STORAGE | | |
| Pond storage capacity | 1,021 | m3 |
| Freeboard storage capacity | - | m3 |
| Pond storage surface area | 900 | m2 |
| Pond storage basal area | 186 | m2 |
| Pond storage catchment area | 900 | m2 |
| Initial pond volume | 0.5 | vol/vol |
| Pan evaporation percentage - winter | 70% | |
| Pan evaporation percentage - autumn | 75% | |
| Pan evaporation percentage - spring | 70% | |
| Pan evaporation percentage - summer | 70% | |
| DISPOSAL | | |
| Pond operating volume | 0.2 | |

| Devenueten | lanuary | February | Marah | Amuli | Mary | luma | Index | A | Contombor | Ostahar | November | December | Annua | l Total | Deveent |
|---|---------|----------|--------|--------|-------|-------|--------|--------|-----------|---------|----------|----------|-------|---------|---------|
| Parameter | January | February | March | April | Мау | June | July | August | September | October | November | December | mm | m3 | Percent |
| | 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 30 | 31 | | | |
| Precipitation (mm) | | | | | | | | | | | | | | | |
| Rainfall (1952) (mm) | 46.4 | 28.0 | 228.0 | 320.7 | 45.6 | 111.4 | 317.4 | 371.3 | 24.4 | 115.1 | 43.1 | 50.1 | 1702 | | 100% |
| Pan Evaporation | | | | | | | | | | | | | | | |
| Evaporation (from SILO) (mm) | 170.9 | 139.6 | 120.8 | 91.2 | 66.9 | 55.3 | 63.6 | 89.2 | 115.9 | 143.4 | 157.6 | 181.5 | 1396 | | 82% |
| Pan evaporation (mm) | 119.6 | 97.7 | 90.6 | 68.4 | 50.2 | 38.7 | 44.5 | 62.4 | 86.9 | 107.6 | 118.2 | 127.1 | 1012 | | 59% |
| Runoff - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Interim cover (flat) | 9.1 | 1.3 | 79.3 | 88.2 | 2.6 | 35.0 | 131.0 | 132.7 | 0.6 | 19.4 | 1.7 | 1.8 | 503 | 23121 | 30% |
| Interim cover (sloped) | 9.5 | 1.4 | 80.4 | 90.7 | 2.8 | 35.7 | 131.9 | 134.7 | 0.7 | 20.4 | 1.9 | 1.8 | 512 | 10594 | 30% |
| Final cap - Option 1 (flat) | 0.6 | 0.0 | 116.8 | 188.1 | 0.0 | 46.6 | 244.0 | 305.6 | 0.0 | 2.7 | 0.0 | 0.0 | 904 | 0 | 53% |
| Final cap - Option 1 (sloped) | 1.1 | 0.0 | 120.5 | 188.5 | 0.0 | 48.5 | 246.4 | 305.5 | 0.0 | 4.1 | 0.0 | 0.0 | 915 | 25664 | 54% |
| Final cap - Option 2 (flat) | 0.0 | 0.0 | 73.0 | 222.0 | 9.3 | 65.1 | 257.4 | 322.1 | 0.0 | 3.5 | 0.0 | 0.0 | 952 | 15144 | 56% |
| Final cap - Option 2 (sloped) | 0.0 | 0.0 | 58.4 | 195.8 | 0.2 | 51.3 | 243.6 | 310.4 | 0.0 | 0.9 | 0.0 | 0.0 | 861 | 19481 | 51% |
| Centre area - Green waste | 3.1 | 0.0 | 125.1 | 216.0 | 4.5 | 60.2 | 257.4 | 320.9 | 0.0 | 14.4 | 0.0 | 0.0 | 1002 | 6310 | 59% |
| Total Runoff (m3/month) | 664 | 86 | 11,962 | 20,550 | 358 | 6,285 | 26,899 | 31,639 | 39 | 1,596 | 116 | 118 | | 100,313 | |
| Evapotranspiration - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 20.0 | 8.3 | 44.4 | 77.5 | 41.0 | 18.3 | 19.5 | 56.7 | 9.9 | 63.3 | 30.6 | 30.2 | 420 | 0 | 25% |
| Interim cover (flat) | 34.8 | 7.5 | 62.1 | 89.7 | 65.2 | 32.6 | 18.7 | 73.7 | 9.1 | 83.3 | 34.1 | 38.1 | 549 | 25247 | 32% |
| Interim cover (sloped) | 34.6 | 7.5 | 62.1 | 89.2 | 64.6 | 32.5 | 18.7 | 73.4 | 9.1 | 83.0 | 26.9 | 41.7 | 543 | 11247 | 32% |
| Final cap - Option 1 (flat) | 41.0 | 27.8 | 82.5 | 77.5 | 55.7 | 35.3 | 34.2 | 69.2 | 23.2 | 99.2 | 50.9 | 41.8 | 638 | 0 | 38% |
| Final cap - Option 1 (sloped) | 40.6 | 27.8 | 82.7 | 73.4 | 55.4 | 34.6 | 33.3 | 68.7 | 22.1 | 98.3 | 50.6 | 41.8 | 629 | 17658 | 37% |
| Final cap - Option 2 (flat) | 46.4 | 27.8 | 81.6 | 71.7 | 48.2 | 43.1 | 43.8 | 67.5 | 35.7 | 115.2 | 93.8 | 42.3 | 717 | 11400 | 42% |
| Final cap - Option 2 (sloped) | 46.4 | 27.7 | 81.5 | 67.3 | 48.7 | 43.0 | 41.4 | 66.6 | 35.8 | 114.8 | 71.1 | 42.3 | 686 | 15538 | 40% |
| Centre area - Green waste | 41.5 | 27.6 | 82.6 | 78.8 | 57.3 | 45.2 | 39.5 | 70.1 | 22.1 | 98.3 | 53.7 | 42.2 | 659 | 4151 | 39% |
| Total Evapotranspiration (m3/month) | 5,504 | 2,527 | 10,127 | 11,187 | 8,119 | 5,089 | 4,063 | 9,859 | 2,744 | 13,352 | 6,987 | 5,683 | | 85,242 | |
| Leachate - Calculated using HELP (mm) | | | | | | | | | | | | | | | |
| Daily cover | 58.1 | 4.2 | 26.0 | 147.2 | 173.1 | 97.2 | 94.9 | 364.1 | 174.9 | 83.7 | 67.6 | 10.9 | 1302 | 0 | 77% |
| Interim cover (flat) | 3.0 | 0.0 | 18.5 | 67.7 | 103.8 | 50.1 | 32.1 | 144.2 | 140.9 | 65.7 | 3.4 | 0.0 | 629 | 28946 | 37% |
| Interim cover (sloped) | 2.2 | 0.0 | 18.0 | 67.7 | 103.0 | 49.3 | 30.9 | 142.2 | 140.3 | 63.5 | 2.2 | 5.2 | 624 | 12925 | 37% |
| Final cap - Option 1 (flat) | 8.1 | 0.0 | 0.0 | 24.5 | 29.6 | 16.5 | 18.0 | 24.9 | 15.0 | 7.3 | 8.2 | 0.0 | 152 | 0 | 9% |
| Final cap - Option 1 (sloped) | 8.0 | 0.0 | 0.0 | 24.2 | 29.8 | 16.3 | 17.1 | 25.6 | 14.8 | 6.7 | 8.6 | 0.0 | 151 | 4240 | 9% |
| Final cap - Option 2 (flat) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Final cap - Option 2 (sloped) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0 | 0 | 0% |
| Centre area - Green waste | 3.5 | 1.9 | 3.5 | 2.4 | 0.5 | 4.0 | 0.0 | 1.4 | 1.6 | 6.3 | 4.1 | 5.1 | 34 | 216 | 2% |
| Total Leachate Collected (m3/month) | 431 | 12 | 1,245 | 5,207 | 7,744 | 3,806 | 2,595 | 10,304 | 9,810 | 4,563 | 470 | 140 | | 46,327 | |
| Other Leachate Sources (m3/month) | | | | | | | | | | | | | | | |
| Open cell | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | |
| Centre area - Transfer station | 16 | 10 | 81 | 114 | 16 | 39 | 112 | 131 | 9 | 41 | 15 | 18 | | 602 | |
| Leachate Storage Pond | | | | | | | | | | | | | | | |
| Rainfall into pond (m3) | 42 | 25 | 205 | 289 | 41 | 100 | 286 | 334 | 22 | 104 | 39 | 45 | | 1,531 | |
| Evaporation from pond (m3) | 65 | 61 | 56 | 62 | 45 | 35 | 40 | 56 | 78 | 97 | 106 | 114 | | 816 | |
| Net Leachate Generation (m3) | 425 | -14 | 1,475 | 5,548 | 7,756 | 3,910 | 2,953 | 10,713 | 9,763 | 4,611 | 417 | 88 | | 47,645 | |







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